# Helium recovery by membrane gas separation using Poly(oacyloxyamide)s (PORAs)

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### Abstract

Poly-o-acyloxyamides (PORAs) derived from a poly(*ortho*-hydroxyamide) from the 2,2'-Bis(3-amino-4-hydroxyphenyl) hexafluoropropane (APAF) diamine, APAF-POHA, have been synthesized and evaluated as gas separation materials. These polymers were made from poly(o-hydroxyamides) by derivatization of the free OH group with an aliphatic acid dichloride or dianhydride that allowed the introduction of acetyl or pivaloyl groups on their structure. All of them showed low-medium thermal stability due to a degradation of the amide moieties and most of them (those synthesized from isophthaloyl dichloride (IPC), 2,2'-bis(4-carboxyphenyl) hexafluoropropane dichloride (6FC) and 4,4'-dicarboxydiphenylsulfone dichloride (DPSC)) showed good mechanical properties.

These poly-o-acyloxyamides have shown good permselectivities for  $He/N_2$  and  $He/CH_4$  separations and very good permeability-selectivity balance for the  $He/CO_2$  separation. The acetyl PORAs showed better permeability versus selectivity balance than the pivaloyl ones. Moreover, selectivity increased while permeability decreased in the sequence:  $6F-APAF \rightarrow IP-APAF \rightarrow DPS-APAF$ 

Intersegmental distances, d-spacing values, were shown to decrease along this sequence obtaining a nice correlation between permeability and d-spacing.

Keywords: Gas separation membranes, Helium separation, Poly(o-hydroxyamide)s (POHAs), Poly(o-acyloxyamide)s (PORAs), d-spacing, Free volume fraction.

### INTRODUCTION

Helium is an inert, low-density gas with a lot of exclusive characteristics which are required for a range of industrial applications and scientific accomplishments. It is the lightest of all gases after hydrogen, it is highly permeable and it has praiseworthy heat transfer properties. It does not become radioactive when exposed to radiation, and remains liquid even near  $OK^1$ . It has been used as a refrigerant in low-temperature devices, as heat transfer agent in nuclear reactors and as a protective and inert atmosphere for purging and pressurizing. It is extensively engaged in shield arc welding technology and leak detection, chromatography, high-field NMR and controlled atmosphere. Other applications are in superconductive, medical, and other advanced technological applications such as space boosters, breathing gas for undersea work, cryogenics, and particularly, applications related to atomic energy<sup>1</sup>.

Helium is the second most generously spread element in the cosmos. But, in spite of this, it is very scarce in the earth's rocks where it is in the ppb range, In the atmosphere it reaches only 5.2 ppm per volume<sup>2</sup>. Opportunely, there are accumulations of helium in natural gas reservoirs from where it can be extracted. Helium is in natural gas reservoirs in concentrations ranging from nearly 0.005% to maxima of approximately about 8.0%. Concentrations over 0.3% are considered to be present only in helium-rich natural gas<sup>1</sup>.

Helium is one of these materials required for the generation, transmission and storage of renewable energy that often would require reflection on what is sustainability. In the case of helium, its fast depletion from natural gas reservoirs, where it accumulated eras ago, without a reserve for future generations, is not defensible<sup>3</sup> and certainly does not conform to the ethical requirements of sustainability. The fusion-energy community habitually defines fusion power as "sustainable" in the ecological sense of the word. But actually helium is required both as a cryogenic gas and as a coolant in fusion plants<sup>2, 4, 5</sup> and it will continue so unless spectacular advances were done in superconductivity at high or medium temperatures.

In the last years prices of helium scaled up<sup>2</sup> going from 50 \$ in 2000 to 160 \$ in 2011 per thousand of cubic feet. A helium shortage would cause anarchy in large areas of the global helium-dependent economy, from medical scanners to solders and including optical fibers and LCD screens manufacturers. Moreover, helium is considered a vital element in strategic industries including aerospace and defence<sup>6, 7</sup>. Due to this strategic character of helium, on October 2, 2013, President Obama in USA signed into law the Helium Stewardship Act of 2013, replacing the Helium Privatization Act of 1996 in order to avoid global shortage of helium with significantly higher prices expected for a limited supply<sup>8</sup>. Although USA has 21 % of global helium reserves, it produces 71 % of the world's helium and is the single largest consumer. Helium almost exclusively in the Asian markets. All these countries own 79 % of the world's reserves although they produce only 29 % of the world's helium<sup>9</sup>.

Extraction of helium from natural gas typically involves three handling steps<sup>6</sup>; the first step is the removal of impurities including water, carbon dioxide, and hydrogen sulphide from the gas performed by absorption or adsorption and/or other extraction processes. The second stage is the extraction of the high-molecular-weight hydrocarbons. The third step is a cryogenic processing, which removes most of the remaining methane gas. The product is a gas rich in helium containing 50 to 70 percent helium, and including mostly nitrogen, argon, neon, and hydrogen. Final purification of helium is normally done using: (1) activated charcoal absorbers at liquid-nitrogen temperatures and high pressure that can produce 99.9999 percent helium or (2) pressure-swing adsorption (PSA) processes that can yield helium with 99.99 percent purity.

Membranes, of course, can compete with low temperature sorption and PSA taking advantage of their modularity and easy escalation, low initial investment costs and easy integration in hybrid processes<sup>10</sup>. Actually, membrane separation for helium has been tried since the early seventies<sup>11, 12</sup>. According to Scholes et al., who recently published a survey on the applications of membranes in natural gas processing<sup>13</sup>,

direct He/CH<sub>4</sub> separation with membranes affronts a major problem because, due to the very low He concentrations in most of the natural gas reservoirs, very high He selectivities of the order of 1000 are required<sup>10</sup>. Although alternatively multimembrane cascade or hybrid processes have been considered<sup>13</sup>, these processes have considerable energy consumption due to the needed recompression of permeate. Because, as mentioned above, the current procedures separate helium along with nitrogen (plus argon and hydrogen), membrane processes could be developed for the combined removal of N<sub>2</sub> and recovery of He from the raw natural gas by using combined N<sub>2</sub>/CH<sub>4</sub> with He/N<sub>2</sub> gas separation membranes without recompression.

Herein, we are presenting some new polymeric materials with promising separation performances for gas pairs that includes He. As it will be shown below, these materials have very high permselectivity for the gas couple  $He/CO_2$ , notable permselectivity for the  $He/N_2$  pair and good selectivity-permeability compromise for the  $He/CH_4$  couple of gases. As mentioned before, He/N<sub>2</sub> and He/CH<sub>4</sub> separations have a strong importance in helium production processes. On the other hand,  $He/CO_2$  separation also is of great interest if, in this case, helium is taken as a surrogate for  $H_2^{14, 15}$ . This assumption of correspondence between He and H<sub>2</sub> is possible because the selectivity for He/H<sub>2</sub> of most of the polymers approaches 1 (going from 0.4 to 1.4)<sup>16</sup>. The H<sub>2</sub>/CO<sub>2</sub> separation is of great interest in CO<sub>2</sub> capture to avoid or control the "Greenhouse Effect" and to take profit of hydrogen. Efficiently separating  $CO_2$  from  $H_2$  is one of the crucial phases in an environmentally responsible practice during energy production from fossil fuels. Petroleum coke, coal, and also biomass, can be gasified to produce syngas (a mixture of CO and H<sub>2</sub>) that can be further reacted with water to produce CO<sub>2</sub> and more H<sub>2</sub>. The high temperature, not so high when cogeneration is used, separation of  $CO_2$  to avoid its entrance in the atmosphere and to take profit of  $H_2$  in combustion and/or in fuel cells, is thus a very interesting challenge<sup>17, 18</sup>.

The polymers synthetized here were poly(*ortho*-acyloxyamides) (PORAs) derived from poly(*ortho*-hydroxyamides) obtained from the reaction of 2,2'-Bis(3-amino-4-hydroxyphenyl)hexafluoropropane (APAF) with several aromatic acid dichlorides and

an ulterior introduction of acetyl or pivaloyl groups on these APAF-POHA by modification reactions.

### 2 EXPERIMENTAL

### 2.1 Materials

The monomer 2,2'-Bis(3-amino-4-hydroxyphenyl)hexafluoropropane (APAF) was purchased from Apollo Scientific (UK) and purified by vacuum sublimation at 225–230 °C.

Terephthaloyl dichloride (TC) and isophthaloyl dichloride (IPC) were bought from Sigma-Aldrich and purified by recrystallization on hexane and a final vacuum sublimation near the melting points of these compounds. The other two aromatic acid dichlorides used, having a SO<sub>2</sub> (DPSC) or a C(CF<sub>3</sub>)<sub>3</sub> group (6FC) linking the aromatic rings, were prepared in our laboratory.

### 2.2 Synthesis

#### A. Synthesis of Acid Dichlorides

The acid dichlorides with hinge groups  $SO_2$  and  $C(CF_3)_3$  were synthesized by reaction of the corresponding diacids with 3-fold mol/acid group of thionyl chloride in the presence of some drops of N,N-dimethylformamide, DMF, as catalyst at 60 °C for 6h. The excess of thionyl chloride was distilled off and the remaining solid was purified by recrystallization in toluene and vacuum sublimation at 160-170°C for dichloride having a  $SO_2$  group, and recrystallization in pentane and subsequent purification by vacuum sublimation at 80-90°C for the monomer having a  $C(CF_3)_3$  group. The scheme of reaction is shown in Figure 1.

Figure 1. Scheme of the synthesis of the dichlorides from diacids.

#### **B.** Synthesis of Polymers

The general procedure for the synthesis of aromatic poly(*ortho*-hydroxyamide)s, POHAs, consisted in dissolving 5 mmol of the APAF diamine in 5 mL of NMP (N-methyl-2-pyrrolidone) or DMA (dimethylacetamide) at room temperature. Afterwards, the solution was cooled to 0°C and then, the necessary amount of trimethylchlorosilane, TMSCI, (20 mmol) and pyridine (20 mmol) were slowly added. Finally, when the sylilation process finished, the temperature of experiment evolved to room temperature and 5 mmol of acid dichloride with 5 mL of solvent were added to the reaction mixture and polycondensation proceeded for 6 hours. The polymer was precipitated and washed with distilled water and dried at 180°C under vacuum to remove occluded solvent.

The preparation of poly(o-acyloxyamide)s, PORAs, was carried out experimentally from the poly(*o*-hydroxyamides) by reaction with pivaloyl chloride or acetic anhydride as indicated in the scheme of Figure 2. Modification reaction was essentially carried out by dissolving the corresponding POHA in DMAc and 1.5 mol of reagent/mol of OH group was added in presence of 1.5 mol of pyridine/mol of OH group at room temperature for 5h. After pouring the solution onto water, modified polymer was collected, washed with water for several times and dried at 100 °C under vacuum overnight.

<sup>1</sup>H spectra were recorded on Varian AV Agilan 400 spectrometer working at 400MHz using as solvent deuterated dimethylsulfoxide, DMSO-d<sub>6</sub>. In order to determine the derivatization degree, samples of 10 mg were used using a relaxation delay higher than 7 s at room temperature. The derivatization degree, d<sub>g</sub>, was calculated by average of the following ratios: ratio between the OH signal (around 9.5 ppm) and all the

aromatic proton signals and as well by determining the ratio between all the aromatic protons and the aliphatic signal associated to the methyl proton of the CH<sub>3</sub>-COO moiety (acetyloxy compound) and the methyl protons of the (CH<sub>3</sub>)<sub>3</sub>C-COO moiety (pivaloyloxy compounds). Both ratios were very alike and the average value was calculated from both measurements. The so obtained derivatization degrees are shown in Table I. It is seen that derivatization for acetyl and pivaloyl polyamides were higher than 74 % and 80%, respectively.

Table I. Derivatization degree of the PORAs obtained from 1H-NMR.

The values of inherent viscosity were much lower for the acetyl polymers than those of the pivaloyl polyamides. However, all of them showed ability of being processed on tough films with mechanical properties able to withstand the high pressure employed in gas separation applications.

### Figure 2. Scheme of poly-o-acyloxyamides PORAs synthetized and studied.

Polyamide POHA and PORA films were prepared by casting a filtered 10% (w/v) solution of polymer onto a glass plate and heating at 90°C overnight. Afterwards, the resulting film was thermally treated in an open oven at 80°C for 6 h, and subsequently kept at 180°C under vacuum overnight.

### 2.3 Membrane Characterization

### A. Attenuated Total Reflectance-Fourier Transform Infra-red Spectroscopy

ATR-FTIR (Attenuated Total Reflectance-Fourier Transform InfraRed spectroscopy) analysis was made at room temperature by using a PerkinElmer Spectrum One infrared spectrometer equipped with an attenuated total reflectance, ATR, accessory. 16 scans taken directly from the films at a resolution of 4 cm<sup>-1</sup> were averaged to get the FTIR spectra

### B. Density and Free Volume Fraction

The densities,  $\rho$ , of the dense membrane films were measured with a Sartorius balance provided with a density kit working according to the Archimedean principle as:

$$\rho = \rho_0 \frac{W_{air}}{W_{air} - W_{liq}} \tag{1}$$

where  $\rho$  is the density of the film,  $W_{air}$  and  $W_{liq}$  are the weights of the film in air and in the auxiliary liquid (in this case isooctane)<sup>19</sup>, and  $\rho_o$  is the density of the auxiliary liquid.

The fraction of free volume, FFV, can be evaluated by:

$$FFV = \frac{V - V_0}{V} = \frac{V - 1.3V_w}{V}$$
(2)

where V is the specific volume, V=1/ $\rho$ , of the polymer at the temperature of interest, and V<sub>0</sub> is the specific volume at 0 K which is estimated as 1.3 times the Van der Waals volume, V<sub>w</sub>. Thus the fractional free volume can be estimated from measurements of the polymer density and a calculation of the Van der Waals volume either from group contribution theory of Bondi<sup>20, 21</sup> or by molecular simulation using an appropriate computational chemistry program.

#### C. Viscosimetry

Inherent viscosities were measured at 25°C with an Ubbelohde viscometer. Ubbelohde viscometers are capillary viscometers. Capillary viscometers are, in general, used for Newtonian, incompressible and wall adherence liquids. The flow inside the capillary is assumed to be under ideal conditions being laminar, incompressible and stationary. Moreover, the specificities of the flow at both the entry and the exit of the capillary are assumed to be negligible and the viscosity to be pressure independent. The time of transit of polymer solutions in NMP with concentrations below 0.5 g/dL was measured and the inherent viscosity was obtained.

#### D. Wide Angle X-ray difraction

Wide-angle X-ray diffraction (WAXD) patterns were recorded at room temperature in the reflection mode by using a Bruker D8 Advance diffractometer provided with a PSD Vantec detector (from Bruker, Madison, Wisconsin). Cu K $\alpha$  radiation ( $\lambda$  = 0.1542 nm)

#### Industrial & Engineering Chemistry Research

was used, operating at 40 kV and 40 mA. The parallel beam optics was adjusted by a parabolic Göbel mirror with horizontal grazing incidence Soller slit of 0.12° and LiF monochromator. The equipment was calibrated with different standards. A step scanning mode was employed for the detector. The diffraction scans were collected within the range of  $2\theta = 3-55^\circ$ , with a  $2\theta$  step of 0.024° and 0.5 s per step.

The average intersegmental distances (d-spacing)<sup>22</sup>, d, can be assessed from the Bragg's law as:

$$n\lambda = 2d \, \operatorname{sen}\theta \tag{3}$$

n being the order number,  $\theta$  the diffraction angle and  $\lambda$  the wave length which corresponds to that of Cu K<sub> $\alpha$ </sub>.

#### E. Differential Scanning Calorimetry

DSC (Differential Scanning Calorimetry) experiments were carried out in a Mettler Toledo (DSC 822e) calorimeter equipped with a liquid nitrogen complement. Disc samples cut from the films were sealed in aluminium pans and heated and cooled in order to monitor the thermal response. The heating protocol was as follows: heating from 25°C to the 250 °C at 10°C/min (this final temperature was employed in order to minimize the degradation process); once the target temperature was reached, the sample was cooled at the maximum cooling to 25°C, held at this temperature for 15 min and reheated at 10°C/min to detect  $T_g$  upto 300 °C.

#### F. Thermo-gravimetric Analysis

TGA (ThermoGravimetric Analysis) was performed using a Thermal Analysis Q500 device. Discs, ranging from 5 to 15 mg in weight, were cut from films and tested. High Resolution (HiRes) mode, with the heating rate automatically adjusted in response to changes in the rate of weight loss, was used with an initial heating rate of 10°C/min under a flux of nitrogen.

#### G. Strain-stress Analyisis

To complete the study on the physical properties of these polymers, the mechanical properties were measured in tension in an MTS Synergie-200 testing machine equipped with a 100 N load cell. Rectangular test pieces of 5 mm width and 25 mm length were tested. A crosshead velocity of 5 mm/min was used. Strain was measured from crosshead separation and tests were conducted at room temperature

#### 2.4 Permselectivity

The permeability, P, for He,  $CH_4$ ,  $N_2$ ,  $O_2$  and  $CO_2$  have been determined by using a permeator with variable pressure (constant volume) operating by the well known *time-lag* method. A illustration of the device used has been shown elsewhere<sup>23</sup>. The measurements have been carried out at 30 °C and at a pressure of 3 bar.

According to the *time-lag* operation method, permeability and diffusivity can be obtained directly from the flow rate into the downstream fixed volume when reaching stationary conditions. Solubility, S, can be, in turn, obtained indirectly from measured diffusivities and permeabilities according to S = P/D.

### RESULTS AND DISCUSSION

### 3.1 Membrane Physicochemical Properties

#### A. ATR-FTIR Spectroscopy

In Figure 3, the ATR-FTIR spectra for the PORAs IP-APAF-Ac and IP-APAF-Pv along with that of the corresponding POHA are shown. Some characteristic for the POHAS can be easily seen:

- **N-H**<sub>st</sub> from 3500 to 3300 cm<sup>-1</sup>.
- O-H<sub>st</sub> from 3500 to3200 cm<sup>-1</sup>. In polymers this peak is usually wide and often split.

- C<sub>ar</sub>-H<sub>st</sub> in the range 3080-3030 cm<sup>-1</sup>. This band appears as wide signal caused by the convolution of multiple energy absorptions.
- C=O<sub>st</sub> symmetric between 1680 and 1670 cm<sup>-1</sup>.
- C<sub>ar-</sub>C<sub>ar</sub> from 1625 to 1575 cm-1 and in the 1525-1475 cm<sup>-1</sup> range<sup>-1</sup>
- N-H δ a weak signal appears in the same zone from 1650 to 1590 cm<sup>-1</sup>.
- **O-H**  $\delta$  in the vibrational plane, from 1450 to 1200 cm<sup>-1</sup>.

In turn, PORAs are characterized by having the following absorption bands:

- Disappearance of the OH associated signal from 2500 to 3600 cm<sup>-1</sup>.
- Appearance of the u<sub>C=0</sub> characteristic of the ester group (both acetyl and pivaloyl) about 1780 cm<sup>-1</sup>.
- Presence of a band caused by the stretching vibration of the link C-O from the ester that is placed around 1150cm<sup>-1</sup>, for the pivaloyl derivatives and around 1200 cm<sup>-1</sup> for acetyl derivatives.

Figure 3. FTIR spectra of the series of PORAs obtained from the POHA IP-APAF. Also, the corresponding POHA is depicted.

#### B. Density and FFV

The measured density and evaluated van der Waals specific volume (by the Bondi method) along with the free volume fraction, obtained according to Equations (1) and (2), are shown in Table II. The free volume fractions were bigger for the pivaloyl derivatives than for the acetyl ones according to the bigger size of the pivaloyl group that in addition decreases the rigidity of the polymer chains reducing the T<sub>g</sub> as will be mentioned below.

Table II. Density, free volume fraction and inherent viscosity of polymers.

### C. Viscosity

The inherent viscosities of the PORAs studied are shown in Table II. As for FFV, there is a clear effect of the higher size of pivaloyl, in this case, increasing the viscosity. It can be settled that for the acetyl PORAs the values of viscosity correspond to medium molecular weight, whereas for PORA-Pv their viscosities (except for the polymer from TC) are high enough to consider that they have high molecular weight. For the sake of comparison the inherent viscosities of the poly(*ortho*-hydroxyamide)s are shown in Table III. As commented above, all the synthesized polymers had enough molecular weight to exhibit film forming properties.

Table III. Inherent viscosities of the precursor POHAs.

#### D. WAXD

Figure 4 shows the diffraction spectra obtained by WAXD for all the PORAs studied. In all cases diffractograms showed no crystallinity peaks, which permit to assert that these structures are amorphous polymers for both the acetyl and pivaloyl PORAs.

#### Figure 4. WAXD analysis of acetyl (a) and pivaloyl (b) PORAs.

The corresponding d-spacings appear in Table IV. In amorphous polymers the values of d can be correlated directly with the size of the free volume elements through which gases diffuse<sup>22, 24</sup>. Note that also, in this case, the bigger size of the pivaloyl group leads to slightly higher intersegmental lengths for the corresponding PORAs.

#### Table IV. WAXD results for the PORAs studied in this work.

The values of FFV and d-spacing seem to be both determined by the size of the added group, linked respectively to the total free volume and to the mean size of the individual holes forming the free volume, which could be correlated as it is depicted in Figure 5. It seems clear that, although it could be otherwise, in our case there is an approximately monotonous increase of total free volume fraction for increasing average size of the individual holes.

*Figure 5. Free volume fraction as a function of intersegmental distance.* 

Such kind of relationships have been recognized as determined by a spreading apart of the chains with larger d-spacing that would cause an increase in free volume to accommodate a packing as tight as possible<sup>24</sup>.

#### E. DSC

The glass transition temperature revealed by differential scanning calorimetry is shown, for the PORAs studied, in Table V.  $T_g$  increases in the sequence

#### IP-APAF<T-APAF <6F-APAF <DPS-APAF

for the pivaloyl PORAs. Although the acetyl derivatives showed always higher  $T_g$  than the pivaloyl ones a similar tendency is followed. Lower  $T_g$  for the pivaloyl samples could be due to a slight disruption of chain rigidity induced by the bulkier pivaloyl groups.

Table V. Thermogravimetric results along with the DSC (Tg) ones for the PORAs studied.

#### F. Thermogravimetry

The onset temperature for mass loss according to thermogravimetric analysis along with the total carbon residues at 800°C,  $R_c$ , and the weight loss from 50 to 300°C,  $W_L$ , are shown in Table V. The corresponding graphs for cumulative and differential mass loss are shown in Figure 6 for the DPS-APAF both pivaloyled and acetyled.

#### Figure 6. TGA analysis for the acetyl (a) and pivaloyl (b) DPS-APAF PORAs.

On analyzing these results, it can be seen that a strong and rapid degradation takes place at temperatures above 250 °C (values for the pivaloyl derivative were slightly higher). The final char yield was low with values lower than 30%. This rapid and relatively medium-temperature weight loss cannot be attributed to a partial formation of polybenzoxazole, which it is observed for ortho-OH polyamides. Details of the degradation mechanism will be commented elsewhere, but it could be commented here that the electron-withdrawing effect of the acyloxy groups lessens the thermal stability of the amide group.

#### G. Mechanical Properties

An example of a strain-stress curve, in this case, for the IP-APAF-Ac and IP-APAF-Pv are shown in Figure 7. Some characteristic<sup>25</sup> parameters are shown on the figure. It is clearly observed that mechanical properties were not very different for the acetyl PORAs respect to the pivaloyl ones, although the later showed higher Young modulus but lower failure strain. It is worth noting that mechanical properties were good except for the case of those made out of the terephthaloyl dichloride that broke at low strains, probably due to a lower polymerization degree. Mechanical properties for acetylated PORAs were high enough despite of the lower molecular weight as indicated by their lower inherent viscosity values.

Figure 7. Stress-strain curves for APAF-IP-Ac and APAF-IP-Pv polymers.

### 3.2 Permeability and Selectivity

The permeability of helium through the PORAs membranes along with their selectivity towards the gas couples He/N<sub>2</sub> and He/CH<sub>4</sub> are shown in Figure 8. In this figure, the gray symbols correspond to the results used by Robeson in his last revision of his permeability-selectivity upper bound<sup>26,16</sup>. Moreover, the zones with more accumulation of polymer representative points are here surrounded by gray lines. Note that the points fit well within the accumulation clouds for the He/N<sub>2</sub> couple. For the He/CH<sub>4</sub> pair the situation was slightly better for some results. This is especially true for DPS-APAF-Ac which has an outstanding selectivity although with a moderate permeability. In both cases, the line of closer approximation to the upper bound showed that clearly the acetyl derivatives have better permselectivities than the pivaloyl ones. The best permeability-selectivity compromise was shown by the 6F-APAF-Ac followed by the IP-APAF-Ac and finally by the DPS-APAF-Ac. In this order, permeability decreases while selectivity is almost constant although evidencing a slight decline.

Figure 8. Robeson plot for  $He/N_2(a)$  and  $He/CH_4(b)$  for all the APAF PORAs studied. Black symbols correspond to the acetyl PORAs while white signs correspond to the pivaloyl ones.

In Figure 9, permeability and selectivity for the  $He/CO_2$  couple of gases are shown, again in a Robeson's plot. In this case the order of decreasing permeability is the same

as for the other pairs of gases but selectivity increases substantially instead of being almost constant. In this case, a decrease in permeability was accompanied with a sharp increase in selectivity. The DPS-APAF-Ac had a quite high selectivity approaching the  $1991^{26}$  upper bound for the He/CO<sub>2</sub> pair, being one of the polymers placed closest to the upper bound<sup>16, 27</sup> in the high selectivity region. This polymer was well placed out of the cloud observed for the most frequent polymers for this couple of gases.

It is worth mentioning that the original 1991 Robeson's bound, as pointed out by Robeson himself<sup>16</sup> would have been mostly conserved if some perfluorinated polymer data had not been considered from literature. These polymers are placed in the medium to high permeability zones of the plot. Moreover selectivities, as high as 300 but having He permeabilities as low as 0.1 Barrer were seen in the 1991 upper-bound<sup>16</sup>.

Figure 9. Robeson plot for  $He/CO_2$  for all the APAF PORAS studied. Black symbols correspond to the acetyl PORAs while white symbols correspond to the pivaloyl ones.

It is known<sup>28</sup> that diffusivity can be correlated with FFV, according to Fujita's theory<sup>29</sup> of diffusion, as:

$$D = A_D e^{-B/FFV}$$
<sup>(4)</sup>

with  $A_D$  and B constants for a given gas and polymer. These factors are correlated with the size and kinetic velocity of the penetrant,  $A_D$ , and the free volume of holes needed for penetrant diffusion, B. Then:

$$P = SA_{D}e^{-B/FFV}$$
(5)

Equation (5) allows the correlation of FFV with permeability and solubility S. Lee<sup>30</sup> originally correlated the permeability of various polymers to their specific free volume. Hensema<sup>31</sup> made an analogous plot including polyimides, polyoxadiazoles and polytriazoles and found different values for A and B. Finally Park and Paul<sup>32</sup> proposed a

general correlation based on more than 100 glassy polymers representing a wide variety of structural types.

Although this correlation has been proved by us for some commercial polymers<sup>33</sup>, it is not perfectly followed for our structures. It seems clear that also free volume distribution and sizes of the narrower necks connecting hole to hole had to be taken into account. Therefore, it is actually possible that smaller total free volumes could include wider necks or throats producing higher diffusivities. In Figure 10 the straight lines correspond to Equation (5). It can be seen that although this correlation is not perfect it is approximately valid for our polymers. Of course, when trying to correlate permeability with FFV according to Eq. (5), the possibility of dealing with different solubility values, S, must be taken into account. Nagel et al.<sup>34</sup> analyzed directly diffusivity, thus solubility should not be disturbing, and they determined that Eq. (4) should be followed. Their results showed again a rough accordance with FFV although their FFV values were achieved from positron annihilation lifetime spectroscopy (PALS) and thus they should be more reliable than any based on the group contribution theory used here.

#### Figure 10. Permeability to all the gases studied as a function of 1/FFV.

Permeability correlated also with other various parameters that characterize chain packing, such as the mean interchain distance (d-spacing deduced from wide-angle X-ray diffraction (WAXD) studies)<sup>35, 36</sup>.

Figure 11 shows the permeability to helium and carbon dioxide along with the selectivity of the He/CO<sub>2</sub> pair as a function of the intersegmental distance, d, obtained from WAXD experiments. It seems clear that permeability increases approximately linearly with d and is higher for the smallest gas (in Figure 11a the molecular size for both gases are shown as stars). The He/CO<sub>2</sub> selectivity increases abruptly when d decreases, which leads to a very high selectivity when d approaches the size of CO<sub>2</sub>. The size volumes showed in Figure 11 were taken from literature<sup>37-40</sup> and they were 2.58 Å for He, 2.96 Å for H<sub>2</sub> and 3.87 Å for CO<sub>2</sub>. The corresponding kinetic diameter, as

taken from sorption data on zeolites, were 2.6 Å for He, 2.9 Å for H<sub>2</sub> and 3.3 Å for CO<sub>2</sub>  $_{38, 41}$ .

Figure 11. Permeability of He and  $CO_2$  (a) and  $He/CO_2$  selectivity (b) as a function of the intersegmental distance (d-spacing). Stars in (a) correspond to the hard sphere molecular diameter of He and  $CO_2$ . The hard sphere size of  $H_2$  is also marked as a vertical dash.

The correlation of permeability and structure has been investigated in depth by Hirayama et al.<sup>42, 43</sup>. They showed that, for several polyimides, the diffusivity versus d-spacing correlation was discrete although this correlation was also poor for the correlation of diffusivity versus 1/FFV. A better but not really complete correlation of permeability with d-spacing and 1/FFV has been found by Bas et al.<sup>44</sup> for several polyimide membranes as a part of an investigation of the correlation of functional versus several structural parameters.

It has been shown that there is a significant increase of intersegmental spacing of various glassy polymers after an exposure to CO<sub>2</sub><sup>45</sup> mostly at high pressures, which produces plasticization. This increase of d-spacing leads to the characteristic increments in permeability. It has also been shown that PVC-POEM grafted copolymers increase d-spacing and permeability when the amount of POEM increases<sup>46</sup>. Nagel et al.<sup>34</sup> measured higher d-spacing in highly selective polymers (glassy poly(amide imide)s, poly(ester imide)s, and polyimides) with high permeabilities and therefore with elevated FFV.

In summary, more accurate correlations of d-spacing, and of FFV, with permeability seem to be obtained when analogue series of polymers are considered. This result seems to confirm that both d-spacing and FFV are not completely descriptive of the polymer and their transport properties. The solubility and distribution of the size of the holes and of the radii of the throats connecting them should be similar in order to achieve a clear correlation of FFV and d-spacing with permeability.

### CONCLUSIONS

Medium thermally stable poly(o-acyloxyamide)s (PORAs) have been obtained and their characteristics studied in detail. Thermal and mechanical properties have been studied confirming the good processability of most of them.

These poly(o-acyloxyamide)s have been shown to have good gas separation properties when Helium is a component of the mixture to be separated, and this finding is especially true for He/CO<sub>2</sub> separations. Attending to the relevance of this separation and also to the similarity of He and H<sub>2</sub> in gas separation, which could be translated to even more significant H<sub>2</sub>/CO<sub>2</sub> separation, it could be inferred that this result is quite promising. Excellent results have been obtained for the He/N<sub>2</sub> separation and good permselectivity for the He/CH<sub>4</sub> separation.

The best selectivity-permeability compromises were attained by the acetyl PORAs whereas the pivaloyl ones showed lower gas separation properties. Selectivity increased and permeability decreased in the sequence

#### 6F-APAF -- IP-APAF -- DPS-APAF

The permeability values versus FFV and as well versus d-spacing have been tested obtaining a nice correlation between permeability and intersegmental, d-spacing, distance.

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### TABLES

<sup>1</sup> H-NMR.					
Polymer	d <sub>g</sub> (%)				
IP-APAF-Ac	82	IP-APAF-Pv	81		
T-APAF-Ac	79	T-APAF- Pv	91		
6F-APAF-Ac	76	6F-APAF- Pv	87		
DPS-APAF -Ac	74	DPS-APAF - Pv	80		

Table I. Derivatization degree of the PORAs obtained from

polymers.					
Polymer	ρ (g/mL)	V <sub>w</sub> (ų)	FFV	η <sub>inh</sub> (dL/g)	
IP-APAF-Ac	1.398	442.20	0.166	0.38	
T-APAF-Ac	1.396	440.74	0.174	0.30	
6F-APAF-Ac	1.422	581.89	0.199	0.46	
DPS-APAF-Ac	1.395	544.58	0.178	0.35	
Polymer	ρ (g/mL)	V <sub>w</sub> (ų)	FFV	η <sub>inh</sub> (dL/g)	
IP-APAFPv	1.252	542.53	0.200	0.80	
T-APAF -Pv	1.277	542.67	0.183	0.33	
6F-APAF -Pv	1.115	680.63	0.335	0.77	
DPS-APAF -Pv	1.340	644.28	0.162	0.67	

Table II. Density, free volume fraction and inherent viscosity of	
polymers.	

Table III. Inherent viscosities of the precursor POHAs.					
Polymer	IP-APAF	T-APAF	6F-APAF	DPS-APAF	
η <sub>inh</sub> (dL/g)	0.79	0.46	0.82	0.56	
η <sub>inh</sub> (dL/g)	0.79	0.46	0.82	0.56	

studied.		
Polymer	20 (deg)	d (Å)
IP-APAF-Ac	18.0	4.9
T-APAF-Ac	16.6	5.3
6F-APAF-Ac	16.0	5.5
DPS-APAF-Ac	18.8	4.7
Polymer	2θ (deg)	d (Å)
IP-APAFPv	16.1	5.5
T-APAF -Pv	16.9	5.3
6F-APAF -Pv	15.8	5.6
DPS-APAF -Pv	17.6	5.0

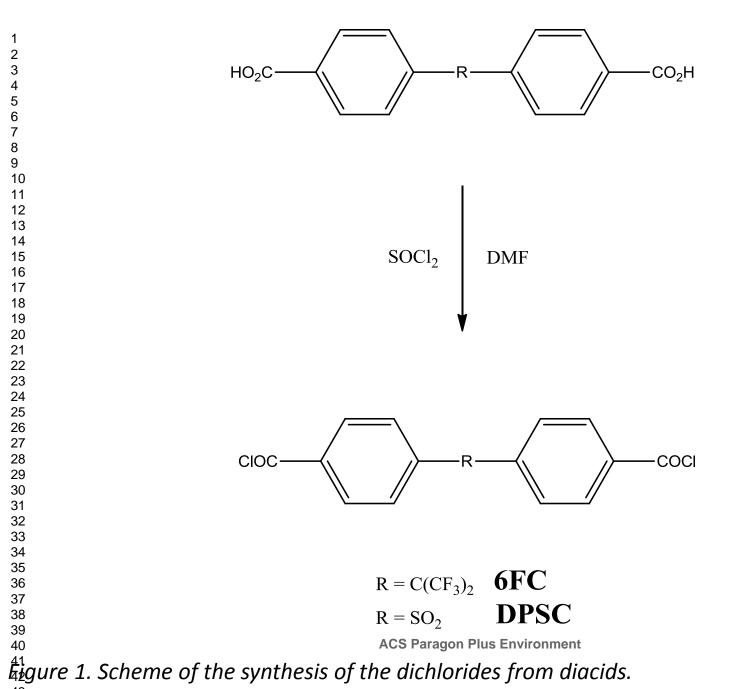
Table	IV.	WAXD	results	for	the	PORAs
studie	d.					

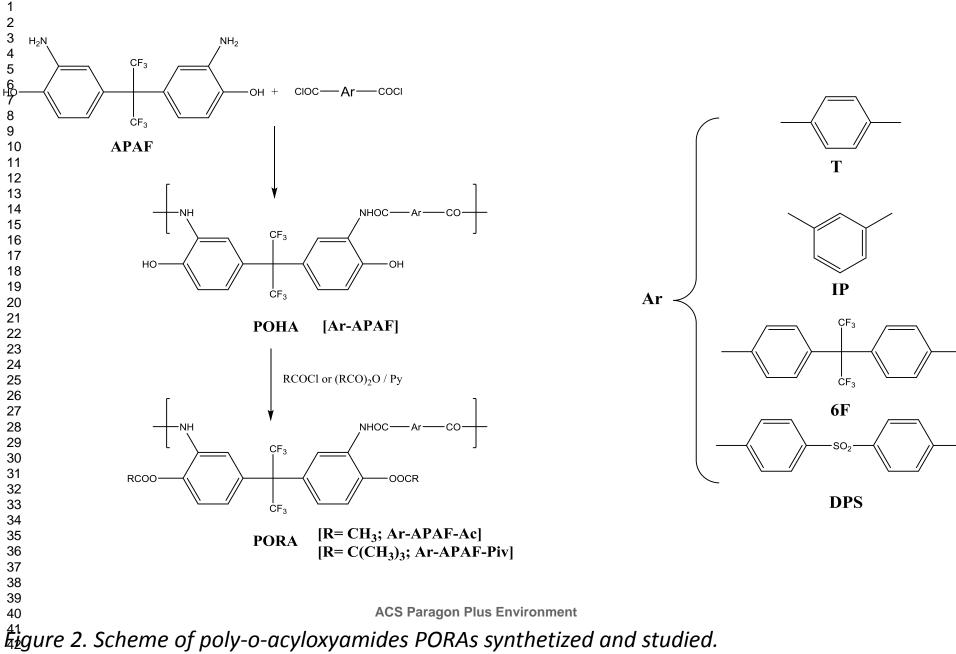
Table V. Thermogravimetric results along with the DSC  $(T_g)$  ones for the PORAs studied.

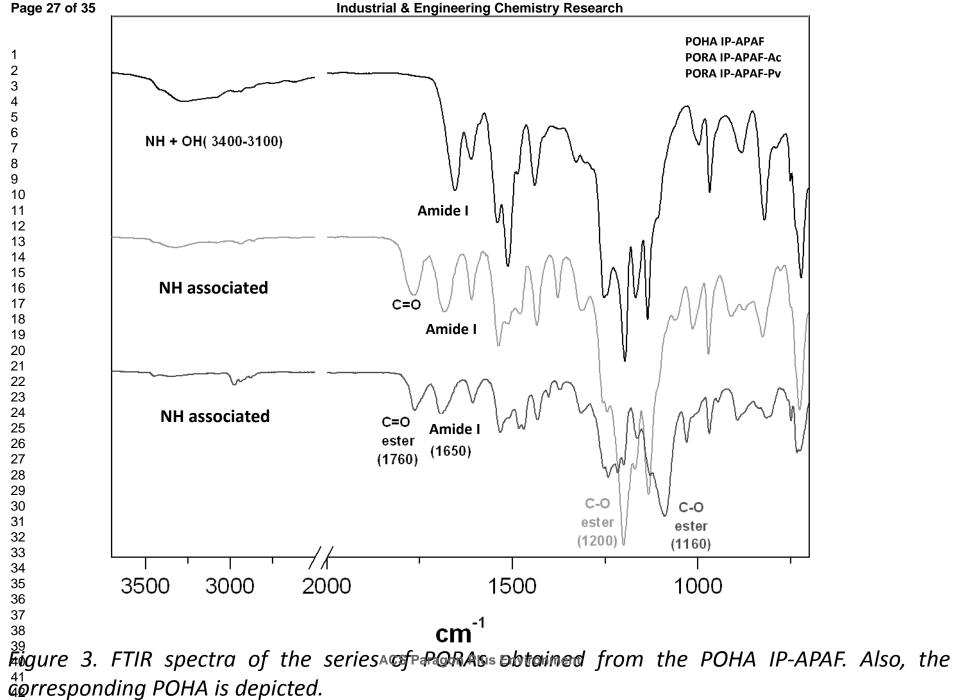
	Temperature (°C)		% R <sub>c</sub>	% WL	
Polymer	T₀ (TGA ONSET)	Tg	Residue (800°C)	weight loss (300°C)	
IP-APAF-Ac	243	167	21	27	
T-APAF-Ac	259	159	22	26	
6F-APAF-Ac	245	196	18	23	
DPS-APAF-Ac	271	183	27	24	
	Temper	atura (°C)	% R <sub>c</sub>	% weight	
Polymer	T <sub>onset</sub>	$T_{g}$	(800°C)	loss	
IP-APAF-Pv	258	130	15	38	
T-APAF -Pv	257	145	20	35	
6F-APAF -Pv	263	153	22	23	
DPS-APAF -Pv	269	168	28	24	

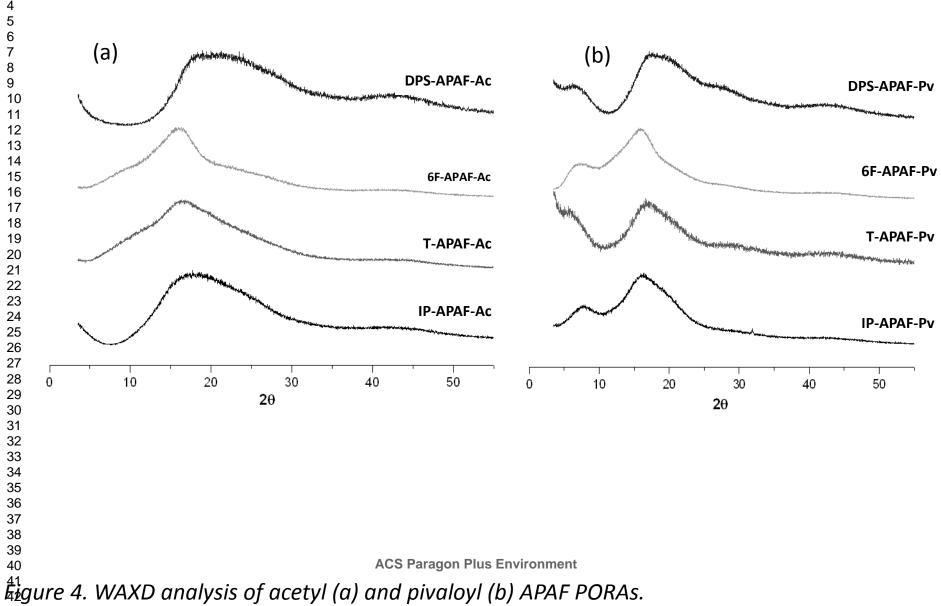
### **FIGURE CAPTIONS**

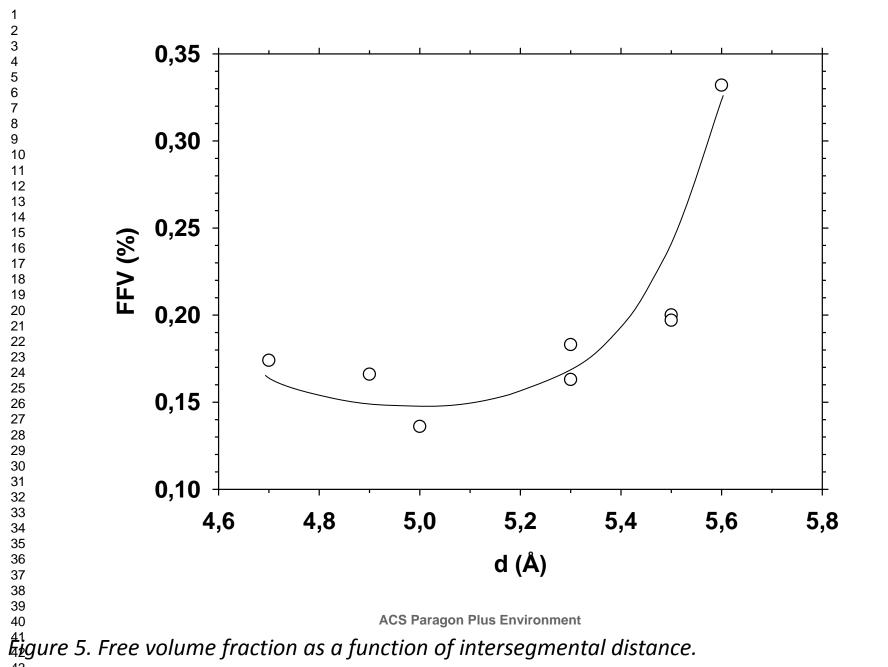
- Figure 1. Scheme of the synthesis of the dichlorides from diacids.
- Figure 2. Scheme of the poly-o-acyloxyamides PORAs synthetized and studied.
- Figure 3. FTIR spectra of the series of PORAs obtained from the POHA IP-APAF. Also, the corresponding POHA is depicted.
- Figure 4. WAXD analysis of acetyl (a) and pivaloyl (b) APAF PORAs.
- Figure 5. Free volume fraction as a function of intersegmental distance.
- Figure 6. TGA analysis for the acetyl (a) and pivaloyl (b) DPS-APAF PORAs.
- Figure 7. Stress-strain curves for IP-APAF- Ac and IP-APAF-Pv polymers.
- Figure 8. Robeson plot for He/N<sub>2</sub> (a) and He/CH<sub>4</sub> (b) for all the APAF PORAs studied. Black symbols correspond to the acetyl PORAs while white signs correspond to the pivaloyl ones.
- Figure 9. Robeson plot for He/CO<sub>2</sub>for all the APAF PORAs studied. Black symbols correspond to the acetyl PORAs while white symbols correspond to the pivaloyl ones.
- Figure 10. Permeability to all the gases studied as a function of 1/FFV.
- Figure 11. Permeability to He and CO<sub>2</sub> (a) and He/CO<sub>2</sub> selectivity (b) as a function of the intersegmental distance (d-spacing). Stars in (a) correspond to the molecular size of He and CO<sub>2</sub>. The hard sphere size of H<sub>2</sub> is also marked as a vertical dash.



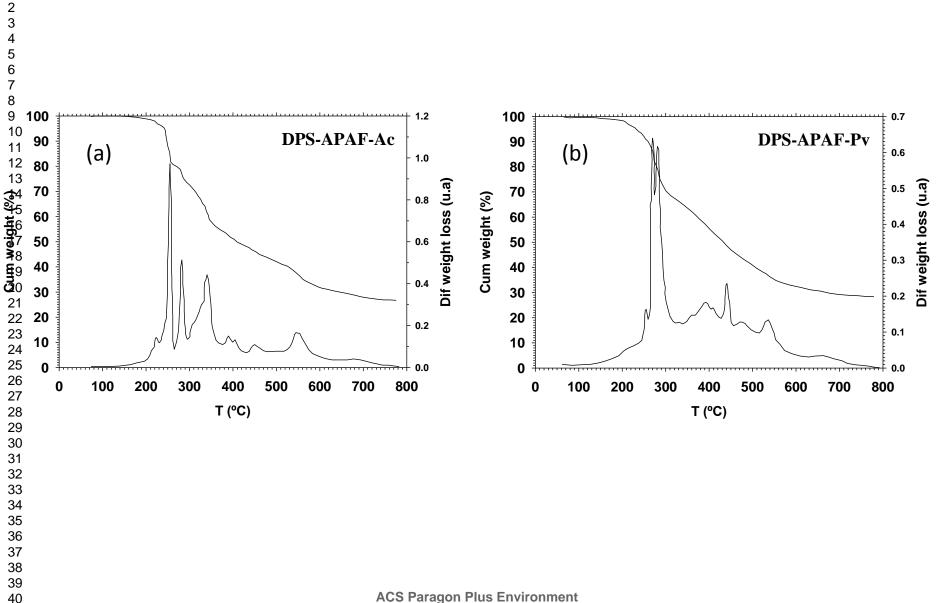






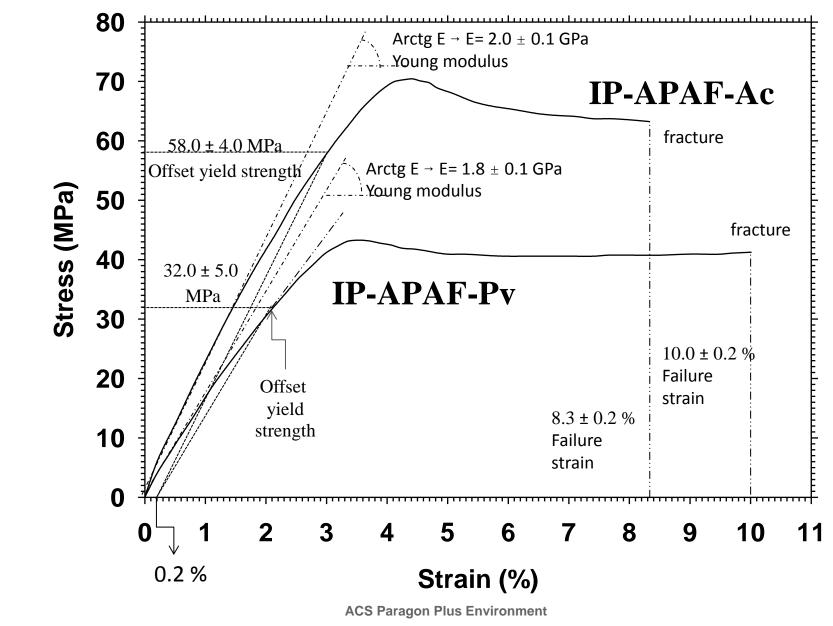


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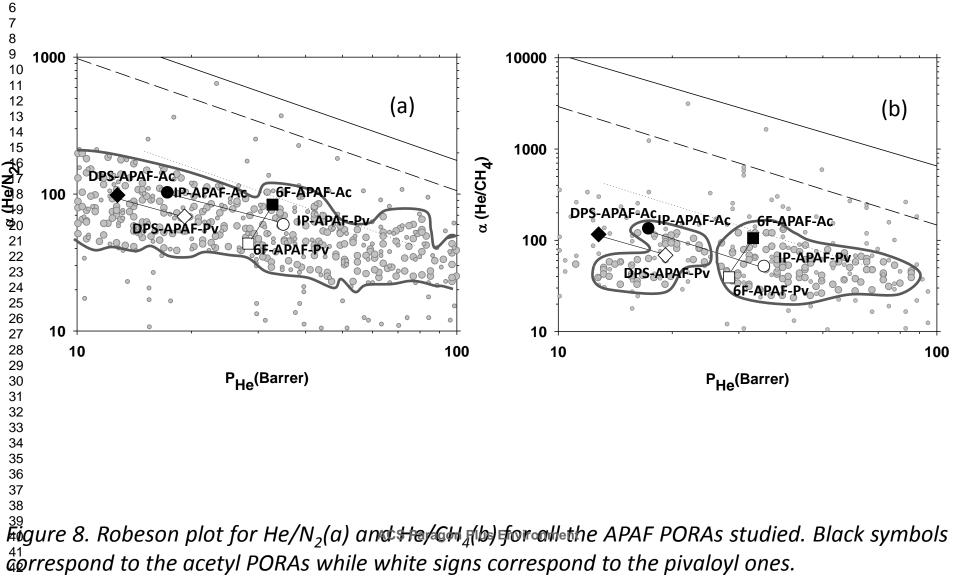


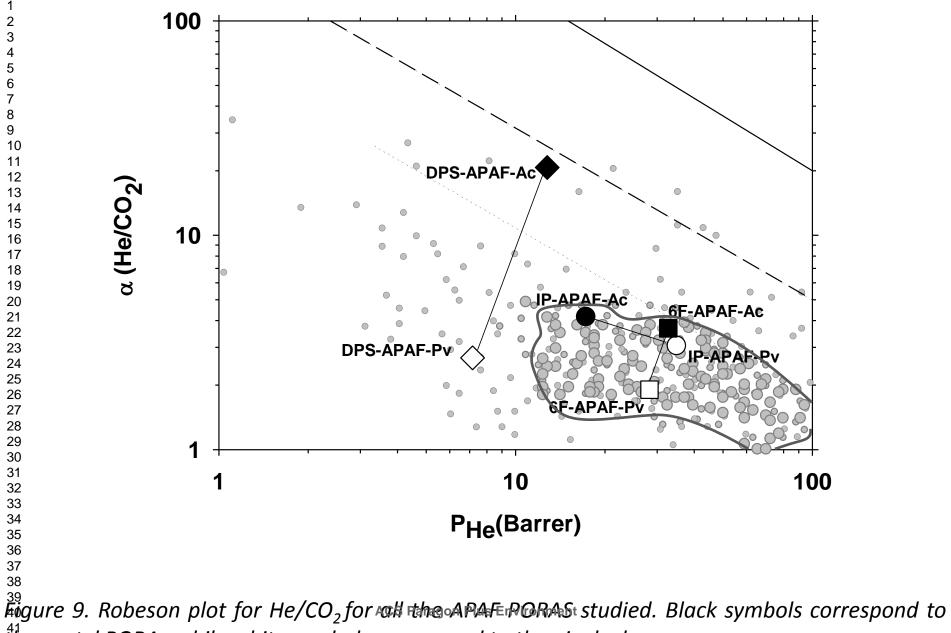
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 $f_{2}^{41}$  gure 6. TGA analysis for the acetyl (a) and pivaloyl (b) DPS-APAF PORAs.

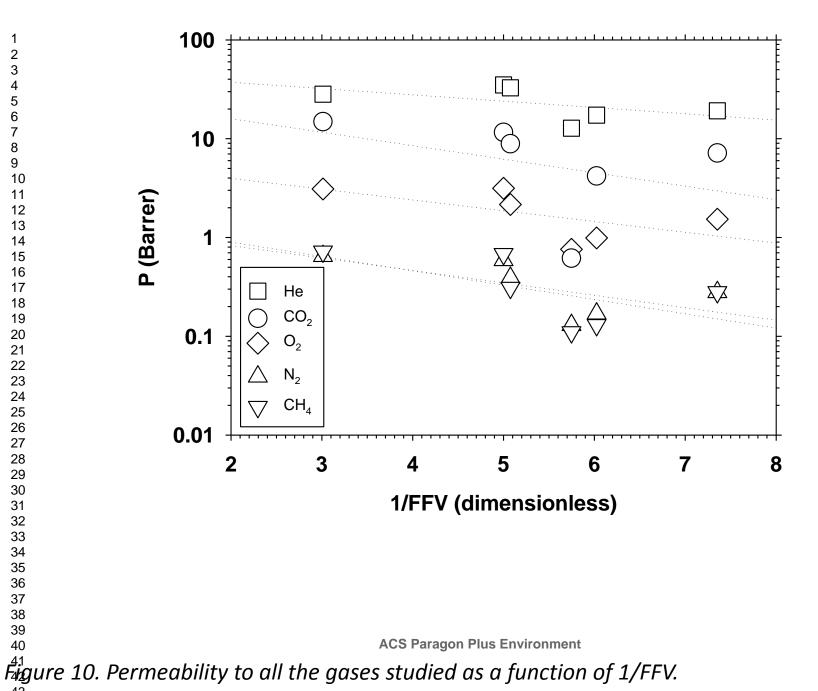


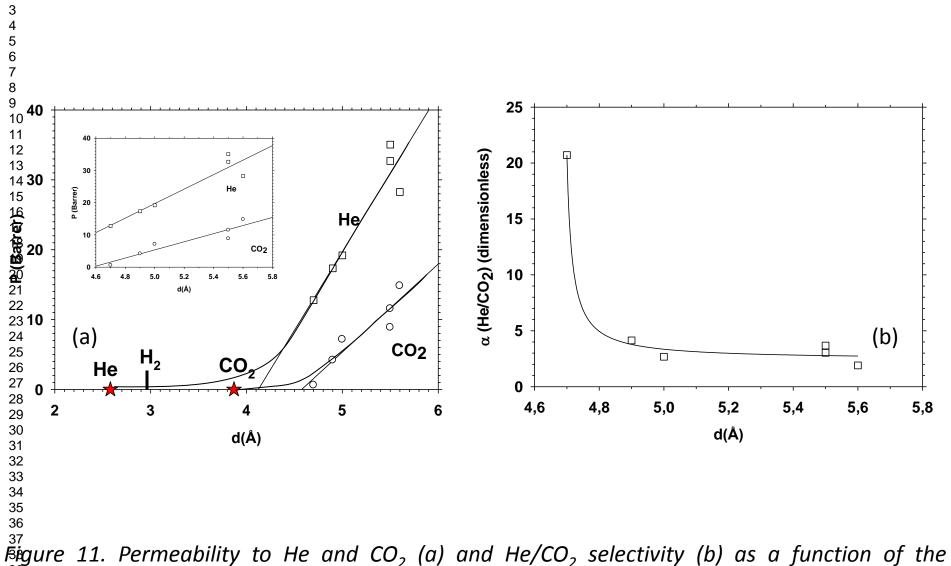
<sup>41</sup> Engure 7. Stress-strain curves for IP-APAF-Ac and IP-APAF-Pv polymers.





the acetyl PORAs while white symbols correspond to the pivaloyl ones.





intersegmental distance (d-spacing). Stors in (a) correspond to the molecular size of He and  $CO_2$ . <sup>39</sup> intersegmental distance (d-spacing). Stors in (a) correspond to the molecular size of He and  $CO_2$ . <sup>41</sup> <sup>41</sup>