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**Enhanced Carbon, Nitrogen and Phosphorus removal  
from domestic wastewater in a novel anoxic-aerobic  
photobioreactor coupled with biogas upgrading.**

Dimas García<sup>1</sup>, Cynthia Alcántara<sup>1</sup>, Saúl Blanco<sup>2</sup>, Rebeca Pérez<sup>1</sup>, Silvia Bolado<sup>1</sup>, Raúl Muñoz<sup>1\*</sup>

1- Department of Chemical Engineering and Environmental Technology, Valladolid University, Dr. Mergelina, s/n, 47011, Valladolid, Spain

2- The Institute of the Environment, La Serna 58 - 24007 León, Spain

\* Corresponding author: [mutora@iq.uva.es](mailto:mutora@iq.uva.es)

# 1. Introduction

The steady increase in human population [1] and industrial activity is generating large amounts of wastewaters and greenhouse gases [2], which represent two of the major environmental challenges to global sustainability nowadays. Domestic and industrial wastewaters and anaerobic digestion effluents are characterized by their high loads of carbon (C), nitrogen (N) and phosphorus (P), which must be treated before discharge into natural water bodies to avoid oxygen depletion, toxicity issues and eutrophication [3]. A wide range of biological and physical/chemical technologies is currently available for carbon and nutrient removal in wastewater treatment plants (WWTPs). Unfortunately, these technologies often entail high investment and operating costs and do not allow for a cost-effective recovery of nutrients due to the low C/N and C/P ratios of most domestic and industrial wastewaters [4][5].

In this context, algal-bacterial processes can support both a low-cost process oxygenation and an enhanced nutrient recovery. The oxygen produced by microalgae during photosynthesis can support the oxidation of organic pollutants and ammonium by aerobic heterotrophs and nitrifiers, respectively, which thus reduces the operating costs and environmental impacts associated with conventional mechanical aeration in WWTPs [6]. On the other hand, the ability of algal-bacterial consortia to assimilate both organic carbon (inherently present in most wastewaters) and inorganic carbon (from the biological oxidation of organic carbon, alkalinity in wastewater or residual carbon dioxide (CO<sub>2</sub>) externally supplied) result in larger biomass productivities and therefore enhanced nutrient recoveries[7]. However, despite the above-mentioned advantages, algal-bacterial processes devoted to wastewater treatment still present severe technical

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limitations that hinder the full-scale implementation of this technology, such as nutrient supply and recycling, gas transfer and exchange [8].

In this regard, although photoautotrophic algal metabolism can enhance N and P recovery in anoxic-aerobic algal-bacterial photobioreactor (AA-ABPh), the alkalinity present in raw wastewaters is low to support a complete nutrient recovery/removal and residual CO<sub>2</sub> sources (such as flue gas) are not always available on-site. In addition, the low hydraulic retention times (HRT) required in algal-bacterial processes to compete with activated sludge systems would limit the development of nitrifying bacterial communities that would eventually support nitrification-denitrification processes during the treatment of wastewaters with low C/N ratios. Finally, the poor sedimentation ability of the microalgae generated in the process often results in effluent total suspended solid concentrations (TSS) above the maximum European Union (EU) discharge limit (50 mg/L), which limits the scale-up of microalgae-based wastewater treatment [9]. In this context, AA-ABPh operated with autoflocculated biomass settling and recycling constitutes an innovative technology capable of overcoming the above mentioned limitations. This technology was successfully evaluated for the treatment of synthetic wastewaters at moderate HRTs but experienced severe inorganic carbon limitations, which ultimately restricted the treatment potential of this innovative technique. Therefore, there is an urgent need to develop novel operating strategies to overcome the above mentioned inorganic carbon limitation and to evaluate the performance of this innovative technology using real domestic wastewater (RDWW) at low HRTs.

1 This work was devised to evaluate the treatment of RDWW in an innovative AA-ABPh  
2 configuration operated with biomass settling and recycling at a HRT of 2 days coupled  
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4 to the simultaneous upgrading of synthetic biogas (in a separate and interconnected  
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6 column). In this system, the supply of biogas (eventually available on-site from the  
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8 anaerobic digestion of the algal-bacterial biomass produced in the process) will provide  
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10 the additional inorganic C source required to boost nutrient removal by assimilation and  
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12 bacterial nitrification to sustain an efficient nitrification-denitrification process [10][11].  
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14 The influence of photosynthetic biogas upgrading on the mechanisms underlying C, N  
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16 and P removal in the anoxic tank and photobioreactor treating RDWW was assessed  
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18 using a mass balance approach. A detailed characterization of the dynamics of  
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20 microalgal and bacterial population structure was conducted using morphological and  
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22 molecular identification tools.  
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## 31 **2. Materials and methods**

### 32 ***2.1. Microorganisms and culture conditions***

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37 The anoxic and aerobic tanks were inoculated with 3.2 g/L of total suspended solid  
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39 (TSS) of an mixture of a microalgal-cyanobacterial consortium (from now on referred to  
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41 as microalgae) from a high rate algal ponds (HRAP) treating diluted vinasse [12] and  
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43 aerobic activated sludge from Valladolid WWTP (Spain). Domestic wastewater was  
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45 collected from a nearby sewer located at Department of Chemical Engineering and  
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47 Environmental Technology of Valladolid University. The average composition of the  
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49 RDWW treated continuously was:  $176\pm 26$  mg/L of dissolved total organic carbon  
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51 (TOC),  $152\pm 34$  mg/L of dissolved inorganic carbon (IC),  $106\pm 9$  mg/L of total nitrogen  
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1 (TN), 93±9 mg/L of N-ammonium (N-NH<sub>4</sub><sup>+</sup>), 39±12mg/L of sulfate (SO<sub>4</sub><sup>2-</sup>) and 33±8  
2 mg/L of P-phosphate (P-PO<sub>4</sub><sup>3-</sup>) (Table 1).  
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## 7 **2.2. Experimental set-up**

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9 Three operational stages (SI, SII and SIII) were carried out in the experimental set-up  
10 below described to evaluate the influence of biogas supply and internal recycling rate on  
11 WWT performance. The experimental set-up during stage I (SI) consisted of an anoxic  
12 tank, with a total working volume of 0.9 L, interconnected to a photobioreactor with a  
13 total working volume of 2.7 L. Both reactors were operated as completely mixed flow  
14 reactors. The anoxic tank was maintained in the dark and magnetically stirred at 320  
15 rpm. The photobioreactor was continuously illuminated for 12 hours/day (05:00h to  
16 17:00h) by LED lamps arranged in a concentric configuration providing an average  
17 light intensity of 392±19 μmol/m<sup>2</sup>·s at the outer wall of the photobioreactor (Figure 1).  
18 Air was introduced during the dark period in order to maintain the dissolved O<sub>2</sub>  
19 concentration in the photobioreactor above non-limiting concentrations [13][14] (Table  
20 1). The temperature and magnetic agitation of the photobioreactor were maintained  
21 constant at 25±1°C and 320 rpm, respectively. During stage II (SII) and stage III (SIII),  
22 the photobioreactor was interconnected to a 0.3 L external absorption column (Ø = 2.54  
23 cm; height = 60 cm) in order to provide an extra source of CO<sub>2</sub> via photosynthetic  
24 biogas upgrading (Figure 1).  
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## 54 **2.3. Experimental design**

1 The HRT and the Sludge Retention Time (SRT) were maintained at 2 days ( $HRT_{\text{anoxic}} =$   
2 0.5 day,  $HRT_{\text{aerobic}} = 1.5$  days) and  $\approx 11$  days, respectively, during the whole experiment  
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4 (Table 1). These short HRTs are required to make algal-bacterial processes competitive  
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6 with activated sludge systems. The experimental design was based on the operational  
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8 limitations identified in previous studies in this AA-ABPh configuration [13][14]. The  
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10 experiment was divided in three operational stages. The internal recycling (IR) flow rate  
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12 from the photobioreactor to the anoxic tank was maintained at 2.8 L/d during SI  
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14 (maintained for 78 days) and SII (maintained for 74 days), while this parameter was  
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16 increased by 30% (3.6 L/d) during SIII (maintained for 56 days) in order to evaluate the  
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18 maximum denitrifying capacity in the anoxic tank to ultimately boost the dissimilatory  
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20 N removal in the experimental system. The external recycling flow rate (ER) from the  
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22 settler to the anoxic tank was maintained at 0.5 L/d during the three operational stages  
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24 (Table 1). The pH in the photobioreactor was maintained between 7.0 and 8.6 during SI  
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26 by daily addition of 1.2 mL of chlorhydric acid (37%), while biogas upgrading into the  
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28 absorption column supplied  $\text{CO}_2$  to overcome the IC limitation encountered during SI  
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30 and to maintain the pH below inhibitory values for bacterial activity ( $< 9$ ) during SII  
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32 and SIII. The synthetic biogas mixture supplied was composed of methane (70%),  
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34 carbon dioxide (29.5%) and hydrogen sulfide (0.5%) (Abello Linde, Barcelona, Spain).  
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36 Biogas was supplied to the absorption column at 2.6 L/d (1.8 ml/min) through a 10  $\mu\text{m}$   
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38 metallic sparger located at the bottom of the column co-currently with a recycling algal-  
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40 bacterial broth stream drawn from the photobioreactor at a liquid to biogas ratio (L/G)  
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42 of 10 (v/v) (Figure 1). Liquid samples of 100 ml were taken twice per week from the  
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44 RDWW, anoxic tank, aerobic tank, settled biomass and effluent to determine  
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46 concentrations of TOC, IC, TN,  $\text{N-NH}_4^+$ ,  $\text{N-NO}_2^-$ ,  $\text{N-NO}_3^-$ ,  $\text{SO}_4^{2-}$ ,  $\text{P-PO}_4^{3-}$  and TSS. pH,  
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48 temperature and dissolved oxygen concentration (DO) were measured daily in both  
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bioreactors. Likewise, the C, N and P content of the algal bacterial biomass was measured under steady state at each operational stage. The sludge volumetric index (SVI) and the maximum biomass settling rate, which were used to monitor the settling characteristics of the algal-bacterial biomass [15], were determined in the anoxic and aerobic bioreactors under steady state at each operational stage. The microalgae population structure was assessed at the end of SI, SII and SIII using biomass samples from the photobioreactor preserved with lugol acid at 5% and formaldehyde at 10%, and stored at 4 °C prior to analysis. Biomass samples from the photobioreactor were collected at the end of each steady state, and immediately stored at -20 °C in order to evaluate the richness and composition of the bacterial communities [14]. Finally, the composition of the biogas at the inlet and outlet of the absorption column was determined twice a week during SII and SIII.

<Table 1>

#### 2.4. Mass balance

The dilution effect in the anoxic tank caused by the internal and external recirculations was considered by calculating a virtual concentration for each parameter in the influent wastewater to the anoxic tank. Hence, the actual C, N and P removals in the denitrification reactor were assessed using the virtual concentrations ( $V_i$ ) for dissolved IC, TOC, N-NH<sub>4</sub><sup>+</sup> and P-PO<sub>4</sub><sup>3-</sup> at the entrance of the anoxic tank according to Eq. (1):

$$V_i \left( \frac{mg}{L} \right) = \frac{(C_{i\ feed} \cdot Q_{feed}) + (C_{i\ aerobic} \cdot Q_{RI}) + (C_{i\ aerobic} \cdot Q_{RE})}{Q_{feed} + Q_{RI} + Q_{RE}} \quad (1)$$

where  $C_{i\ feed}$  and  $C_{i\ aerobic}$  represent the dissolved concentrations of the parameter “ $i$ ”= TOC, IC, TN, N-NH<sub>4</sub><sup>+</sup> and P-PO<sub>4</sub><sup>3-</sup> in the RWW and the photobioreactor, respectively,

1 while  $Q_{\text{feed}}$  represents the RDWW flow rate,  $Q_{\text{RI}}$  the internal recirculation flow rate and  
2  $Q_{\text{RE}}$  the external recirculation flow rate.  
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8 An overall mass balance to the anoxic-aerobic photobioreactor was conducted for TOC,  
9 IC, TN,  $\text{N-NH}_4^+$  and  $\text{P-PO}_4^{3-}$  based on their average concentrations under steady state  
10 conditions for each operational stage. The validity of the instrumental and analytical  
11 methods was thus assessed by means of the mass recovery factors for the parameter “ $i$ ”  
12 according to Eq. (2) [14]:  
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$$21 \quad M_i \text{ Recovery (\%)} = \frac{(M_{i \text{ rem}})_{\text{anox}} + (M_{i \text{ rem}})_{\text{photobior}} + (M_i)_{\text{effl}}}{(M_i)_{\text{RWW}}} \cdot 100 \quad (2)$$

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25 where  $(M_{i \text{ rem}})_{\text{anoxic}}$  and  $(M_{i \text{ rem}})_{\text{photobior}}$  represent the mass flow rate (g/d) of the parameter  
26  $i = \text{TOC, IC, TN, N-NH}_4^+$  and  $\text{P-PO}_4^{3-}$  removed in the anoxic tank and photobioreactor,  
27 respectively.  $M_{i \text{ effl}}$  and  $M_{i \text{ RWW}}$  represent the mass flow rate (g/d) of the parameter in the  
28 treated effluent and RWW, respectively.  
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37 The removal efficiencies herein reported for each tank refer to the individual  
38 contribution of the anoxic and photobioreactor units to the overall removal of the inlet  
39 loading for each monitored parameter.  
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## 47 **2.5. Analytical procedures**

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50 The light intensity was measured as photosynthetically active radiation (PAR) using a  
51 LI-250A light meter (LI-COR Biosciences, Germany). Biogas composition was  
52 determined using a Bruker 430 GC-TCD (Palo Alto, USA) equipped with a CP-  
53 Molsieve 5A (15 m × 0.53 mm × 15 μm) and a CP-Pora BOND Q (25 m × 0.53 mm ×  
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15  $\mu\text{m}$ ) columns. The injector, detector and oven temperatures were maintained at 150 °C, 175 °C and 40 °C, respectively. Helium was used as the carrier gas at 13.7  $\text{cm}^3/\text{min}$ [16]. TOC, IC and TN concentrations were measured using a TOC-V CSH analyzer equipped with a TNM-1 module (Shimadzu, Japan).  $\text{N-NH}_4^+$  was measured using the Nessler analytical method [15] in a U-2000 spectrophotometer (Hitachi, Japan), while  $\text{NO}_2^-$  and  $\text{NO}_3^-$  were determined by the cadmium reduction column method [15].  $\text{P-PO}_4^{3-}$  and  $\text{SO}_4^{2-}$  were analyzed by high performance liquid chromatography-ion chromatography (HPLC-IC) with a Waters 515 HPLC pump coupled with a Waters 432 ionic conductivity detector and equipped with an IC-Pak Anion HC (150 mm  $\times$  4.6 mm) waters column. A 510 pH meter (EUTECH Instrument, The Netherlands) was used for pH determination. DO concentration and temperature were recorded using an OXI 330i oximeter (WTW, Germany). The determination of the TSS concentration, SVI and settling rate were conducted according to Standard Methods [15]. The analysis of the C and N biomass content was carried out using a LECO CHNS-932 elemental analyzer with pre-dried and grinded algal-bacterial biomass. The content of P in the biomass was measured using a 725-ICP Optical Emission Spectrophotometer (Agilent, USA) at 213.62 nm. The identification, quantification and biometry measurements of microalgae were conducted by microscopic examination (OLYMPUS IX70, USA) of the algal-bacterial cultivation broths according to Phytoplankton Manual [17].

Genomic DNA was extracted using the protocol described in the Fast® DNA Spin Kit for Soil (MP Biomedicals, LLC) handbook. The V6-V8 regions of the bacterial 16S ribosomal ribonucleic acid (rRNA) genes were amplified by Polymerase Chain Reaction (PCR) analysis using the universal bacterial primers 968-F-GC and 1401-R

1 (Sigma-Aldrich, St. Louis, MO, USA; [18]). The PCR mixture contained 1  $\mu\text{L}$  of each  
2 primer (10 ng  $\mu\text{L}^{-1}$  each primer), 25  $\mu\text{L}$  of BIOMIX ready-to-use 2 reaction mix  
3 (Bioline, Ecogen), 2  $\mu\text{L}$  of the extracted DNA and Milli-Q water up to a final volume of  
4 50  $\mu\text{L}$ . The PCR thermo-cycling program consisted of 2 min of pre-denaturation at  
5 95°C, 35 cycles of denaturation at 95°C for 30 s, annealing at 56°C for 45 s, and  
6 elongation at 72°C for 1 min, with a final 5-min elongation at 72°C. The denaturing  
7 gradient gel electrophoresis (DGGE) analysis of the amplicons was performed with a D-  
8 Code universal mutation system (Bio Rad Laboratories) using 8% (w/v) polyacrylamide  
9 gels with a urea/formamide denaturing gradient of 45 to 65%. DGGE running  
10 conditions were applied according to Roest et al. (2005) [19]. The gels were stained  
11 with GelRed Nucleic Acid Gel Stain (biotium) for 1 h. The most relevant bands were  
12 excised from the DGGE gel in order to identify the bacteria present in the samples,  
13 resuspended in 50  $\mu\text{L}$  of ultrapure water and maintained at 60 °C for 1hour to allow  
14 DNA extraction from the gel. A volume of 5  $\mu\text{L}$  of the supernatant was used for  
15 reamplification with the original primer set. Before sequencing, PCR products were  
16 purified with the GenElute PCR DNA Purification Kit (Sigma-Aldrich, St. Louis, MO,  
17 USA). DGGE profiles were compared using the GelCompar IITM software (Applied  
18 Maths BVBA, Sint-Martens-Latem, Belgium). After image normalization, bands were  
19 defined for each sample using the bands search algorithm within the program. The peak  
20 heights in the densitometric curves were also used to determine the Shannon-Wiener  
21 diversity index (H). Therefore, this index reflects both the sample richness (relative  
22 number of DGGE bands) and evenness (relative intensity of every band). It ranges from  
23 1.5 to 3.5 (low and high species evenness and richness, respectively) and can be  
24 calculated according to Eq. (3)[20]:  
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$$H = -\sum [P_i \ln(P_i)] \quad (3)$$

Where H is diversity index and  $P_i$  is the importance probability of the bands in a lane ( $P_i = n_i/n$ , where  $n_i$  is the height of an individual peak and n is the sum of all peak heights in the densitometric curves). Similarity indices of the compared profiles were calculated from the densitometric curves of the scanned DGGE profiles by using the Pearson product–moment correlation coefficient [21]. The taxonomic position of the sequenced DGGE bands was obtained using the RDP classifier tool (50% confidence level) [22]. The closest cultured and uncultured relatives to each band were obtained using the BLAST search tool at the NCBI (National Centre for Biotechnology Information) [23]. The sequences generated from this work are deposited in GenBank under accession numbers KU854389-KU854421.

## 2.6. Statistical analysis

The data displayed in Table 1, Figure 2 and Figure 7(c) correspond to the mean  $\pm$  standard deviation of the target parameters during steady state at each operational stage. A one-way ANOVA analysis was performed to assess any significant difference between the settling rate of the biomass from the anoxic reactor and the photobioreactor using Excel (Microsoft, USA). A Pearson correlation analysis was conducted to determine the similarity indexes among the population established during steady state operation.

## 3. Results and Discussion

The mass balance calculations over the 208 days of operation showed recoveries for TOC, IC, TN and  $P\text{-PO}_4^{3-}$  of  $100\pm 1\%$ ,  $99\pm 4\%$ ,  $100\pm 5\%$  and  $100\pm 14\%$ , which validated

1 the analytical and instrumental methodologies used in this study. This mass balance  
2 approach allowed to better understand the symbiosis between microalgae and bacteria in  
3 this novel anoxic-aerobic algal-bacterial photobioreactor configuration [14], by  
4 quantifying the extent of the mechanisms involved in C, N and P removal in each  
5 reactor.  
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11 The overall removal efficiency of organic matter measured as TOC under steady state  
12 operation averaged  $89\pm 2\%$  along the 3 operational stages at 2 days of HRT due to the  
13 high photosynthetic oxygenation capacity and denitrification activity of the system. In  
14 this context, while the DO concentration in the anoxic tank remained close to  $0 \text{ mg O}_2/\text{L}$   
15 (thus supporting an efficient denitrification since the  $\text{O}_2$  carried out by the internal  
16 recycling was lower than  $\text{O}_2$  demand of the RDWW), the DO in the photobioreactor  
17 fluctuated from 15 and  $32 \text{ mg O}_2/\text{L}$  during illuminated periods to 1.5 and  $7 \text{ mg O}_2/\text{L}$   
18 during dark periods in the photobioreactor (supplementary material Figure S1). These  
19 oxygen concentrations were sufficient to satisfy the bacterial demand from  $\text{NH}_4^+$  and  
20 TOC oxidation in the photobioreactor. The organic matter removal recorded in this  
21 study was similar to that typically achieved in conventional activated sludge systems  
22 (COD-REs of 85-90%) and in conventional HRAPs treating domestic wastewater  
23 (COD-REs 81-88%). The high light intensity used in this lab-scale study to boost  
24 microalgae photosynthetic activity ( $392\pm 19 \mu\text{mol}/\text{m}^2\cdot\text{s}$ ) supported an efficient overall  
25 steady state IC removal ( $95\pm 4\%$ ) mainly based on microalgae assimilation, nitrification  
26 representing a minor IC removal mechanism ( $\approx 4.1\%$  of the total IC input).  
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53 On the other hand, the average TN removal during SI under steady state operation  
54 accounted for  $38\pm 6\%$  with average  $\text{NH}_4^+$  removals of  $39\pm 9\%$ . This low TN-RE was due  
55 to the low efficiency of  $\text{NH}_4^+$  nitrification during SI as a result of a severe IC limitation.  
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Biogas supplementation in SII and SIII overcame this limitation and promoted steady state removals of TN and  $\text{NH}_4^+$  of  $81\pm 3\%$ ,  $97\pm 2\%$ , respectively, at a HRT of 2 days.  $\text{NH}_4^+$  nitrification in the photobioreactor was the key step to ensure an efficient nitrogen removal in the anoxic tank via denitrification, despite  $\text{NH}_4^+$  oxidation during SI was limited by the active photosynthetic IC uptake by microalgae. Comparable TN-REs ranging from 68% to 85% and N- $\text{NH}_4^+$ -REs of 80-93% are typically achieved in  $\text{CO}_2$ -supplemented HRAPs treating domestic wastewater but at HRTs of 3-7 days, with nitrogen assimilation into biomass and  $\text{NH}_3$  stripping identified as the main nitrogen removal mechanisms [24]. Lower TN-REs ranging from 57% to 73% are often achieved in HRAPs during the treatment of domestic sewage without  $\text{CO}_2$  supplementation at HRTs of 3-10 days, which highlights the superior performance of our two-stage photobioreactor [25]. In addition, the values hereby obtained for nitrogen removal were comparable with the removal efficiencies of  $\approx 80\%$  typically reported in nitrification-denitrification activated sludge plants, although conventional WWTPs operate at 0.5-1 day of HRT [26].

Finally, average orthophosphate removal efficiencies of  $59\pm 17\%$  were recorded under steady state operation in SI. However, the supplementation of biogas resulted in an enhanced biomass growth and therefore in a slight increase in  $\text{P-PO}_4^3$ -REs up to steady state values of  $67\pm 13\%$  and  $60\pm 6\%$  in SII and SIII, respectively. Bioassimilation into algal-bacterial biomass was likely the main phosphorous removal mechanism since pH values fluctuated from 6.8 to 9.4 during illuminated periods and from 6.4 to 8.1 during the dark periods in the photobioreactor (supplementary material Figure S1). The average pH values recorded along the entire experiment were likely not sufficient to support phosphate precipitation, which has been shown to occur at pHs  $> 9.0$  [6][27]. The P-

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PO<sub>4</sub><sup>3-</sup>-REs here obtained (59 - 67%) were similarly those typically reported in HRAPs (50% to 75%) at significantly higher HRTs (3 – 7 days) and activated sludge processes at HRTs of 0.5 - 1 days [24]. However, the volumetric PO<sub>4</sub><sup>3-</sup> removal rates achieved were superior based on the fact that the phosphate concentration in the RWW used in this study (33±8 mg P/L) was ≈ 5 times higher than the P-PO<sub>4</sub><sup>3-</sup> concentrations typically present in medium strength WW (≈ 7 mg P/L)[28] (Table 1).

Finally, the high robustness of this process configuration should be highlighted based on the consistent effluent concentrations of TOC, IC, NH<sub>4</sub><sup>+</sup>, TN, PO<sub>4</sub><sup>3-</sup> despite the inherent variations of these parameters in RDWW.

### 3.1. *Carbon and nutrient removal in the anoxic reactor*

The overall removal efficiencies of TOC in the anoxic reactor accounted for 77±4% under steady state operation, with values of 77±4%, 76±6% and 79±3% for SI, SII and SIII, respectively (Figure 2a). This heterotrophic TOC removal (organic matter acting as electron donor) resulted in steady state concentrations of 27±5 mg/L in the anoxic tank regardless of the operational stage [29]. On other hand, a negative IC removal efficiency of -14±13% was recorded during SI as a result of CO<sub>2</sub> production from TOC oxidation in the anoxic tank (mainly driven by the use of O<sub>2</sub> as electron acceptor, which represented 67% of the total e<sup>-</sup> acceptor consumption during SI) and the absence of a significant CO<sub>2</sub> stripping due to the overall CO<sub>2</sub> limitation in the process (Figure 2b). The slightly higher aqueous CO<sub>2</sub> concentration in the anoxic tank during SII and SIII mediated by biogas scrubbing supported a desorption of CO<sub>2</sub> from the anoxic tank, resulting in IC REs of 29±12% and 30±6%, respectively.

< Figure 2 >

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TN-REs in the anoxic tank increased from  $18\pm 8\%$  in SI to  $50\pm 6\%$  and  $50\pm 7\%$  in SII and SIII, respectively (Figure 2c). This increase in TN removal was likely induced by the enhanced nitrification in the photobioreactor mediated by biogas supplementation, which ultimately promoted  $\text{N-NO}_2^-$  and  $\text{N-NO}_3^-$  reduction in the anoxic tank using the organic matter present in the influent wastewater. In fact,  $\text{N-NO}_2^-$  and  $\text{N-NO}_3^-$  represented the main  $e^-$  acceptors in SII and SIII, with a contribution to TOC oxidation of 56% and 60%, respectively. The steady state removals of  $\text{N-NH}_4^+$  remained low at  $6\pm 14\%$ ,  $9\pm 11\%$  and  $2\pm 7\%$  during SI, SII and SIII, respectively.  $\text{NH}_4^+$  removal in the anoxic tank was due to biomass assimilation mediated by heterotrophic TOC removal, which remained constant regardless of the operational stage (Figure 2d).  $\text{N-NO}_2^-$  concentrations in the anoxic tank under steady state operation were negligible ( $0.01\pm 0.01$  mg/L,  $0.03\pm 0.05$  and  $0.41\pm 0.68$  in SI, SII and SIII, respectively). Likewise,  $\text{N-NO}_3^-$  concentrations recorded in the anoxic tank in SI, SII and SIII were  $0.04\pm 0.03$ mg/L,  $0.14\pm 0.15$ mg/L and  $0.73\pm 1.25$ mg/L, respectively (Figure 3). These findings confirmed that both  $\text{NO}_2^-$  and  $\text{NO}_3^-$  derived from the photobioreactor and settler via the internal and external recirculations were efficiently reduced.

< Figure 3 >

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Negative overall  $\text{P-PO}_4^{3-}$ -REs of  $-17\pm 31\%$  were recorded in the anoxic tank under steady state operation, with  $\text{P-PO}_4^{3-}$  removals of  $-14\pm 36\%$ ,  $-18\pm 29\%$  and  $-20\pm 25\%$  during SI, SII and SIII, respectively (Figure 2e). These negative  $\text{P-PO}_4^{3-}$ -REs indicated that P was released by the algal-bacterial consortium in the absence of an  $e^-$  acceptor (nitrite, nitrate and dissolved oxygen) during SI, SII and SIII, respectively. In this context, recent studies have reported the ability of microalgae to accumulate non-structural  $\text{P-PO}_4^{3-}$  under aerobic conditions, which is then released in the absence of  $e^-$  acceptor

1 (similarly to phosphate accumulating organisms, PAOs) [30][31]. In addition, the  
2 DGGE-sequencing analysis revealed the presence of heterotrophic bacteria with the  
3 ability to accumulate energy in the form of polyphosphate under excess of  $e^-$  acceptor  
4 and use this energy under anoxic conditions with the subsequent release of  $PO_4^{3-}$  to the  
5 culture medium. Hence, PAOs from the genus *Acinetobacter* (SI, SII and SIII),  
6 *Luteolibacter* (SI, SII and SIII), *Thauera* (SII and SIII), *Pseudomonas* (SIII), and  
7 *Aeromonas* (SI and SIII) were identified (supplementary materials Table S1) [29][32].  
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### 19 **3.2. Carbon and nutrient removal in the photobioreactor**

20 The TOC-REs under steady state operation in the photobioreactor averaged  $12\pm 5\%$   
21 regardless of the operational stage as a result of the efficient removal of organic matter  
22 in the anoxic tank (Figure 2a). The consistent concentrations of TOC  $19\pm 3$  mg/L in the  
23 effluent over the entire experiment allowed us to estimate the fraction of non-  
24 biodegradable organic matter in the influent RWW to 11%. IC-REs in the  
25 photobioreactor under steady state condition accounted for  $86\pm 27\%$  as a result of the  
26 intensive photosynthetic activity during the illuminated period along the three  
27 operational stages in the photobioreactor (Figure 2b). IC was almost completely  
28 depleted during the SI (supplementary material Figure S2b). The occurrence of IC  
29 limitation during SI supported the addition of biogas in order to supply an additional  
30  $CO_2$  source. Even under  $CO_2$  supplementation, high IC-REs of  $63\pm 10\%$  and  $62\pm 7\%$   
31 were recorded during SII and SIII, respectively. The enhanced IC availability mediated  
32 by biogas upgrading entailed an increase in the concentration of algal-bacterial biomass.  
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52 Low TN-REs of  $20\pm 7\%$  were recorded under SI steady state, which increased up to  
53  $30\pm 7\%$  and  $32\pm 9\%$  in SII and SIII, respectively, as a result of the higher biomass  
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1 production induced by biogas supplementation (Figure 2c). Likewise, while IC  
2 limitation mediated low N-NH<sub>4</sub><sup>+</sup>-REs (33±20%) during SI, the increase in nitrification  
3 activity supported by CO<sub>2</sub> supplementation increased N-NH<sub>4</sub><sup>+</sup>-REs up to 89±11% and  
4 96±7% in SII and SIII, respectively (Figure 2d and supplementary material Figure S2d).  
5 N-NO<sub>2</sub><sup>-</sup> was the dominant form of oxidized nitrogen (N-NO<sub>2</sub><sup>-</sup> = 5.6±4.0 mg/L vs N-NO<sub>3</sub><sup>-</sup>  
6 =0.9±0.9 mg/L) during SI (Table 1 and Figure 3). CO<sub>2</sub> supplementation via biogas  
7 upgrading promoted nitrification, which resulted in a decrease in N-NO<sub>2</sub><sup>-</sup> concentration  
8 to 3.1±3.8 mg/L concomitant with an increase in N-NO<sub>3</sub><sup>-</sup> concentration up to 8.9±5.5  
9 mg/L in SII [29]. Likewise, an almost complete nitrification was achieved during steady  
10 SIII, with N-NO<sub>3</sub><sup>-</sup> and N-NO<sub>2</sub><sup>-</sup> of 13.0±3.2 mg/L and 1.1±1.8 mg/L of N-NO<sub>2</sub><sup>-</sup>,  
11 respectively.  
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29 The overall steady state P-PO<sub>4</sub><sup>3-</sup>-REs in the photobioreactor accounted for 80±39%,  
30 with values of 73±49%, 85±28% and 81±29% in SI, SII and SIII, respectively (Figure  
31 2e). P assimilation into algal-bacterial biomass was the most likely removal mechanism  
32 in the photobioreactor based on the range of pH values recorded during illuminated  
33 periods (6.8-9.4) and (6.4-8.1) during the dark periods in SII and SIII.  
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### 44 **3.3. Biomass concentration and sludge volumetric index**

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46 TSS concentration in the anoxic tank increased from 1519±252 mg TSS/L in SI to  
47 3113±361 mg TSS/L and 2480±309 mg TSS/L during SII and SIII, respectively (Table  
48 1 and Figure 4a). Likewise, biomass concentration in the aerobic tank under steady state  
49 operation accounted for 1216±260 mg TSS/L, 2854±324mg TSS/L and 2047±186 mg  
50 TSS/L in SI, SII and SIII, respectively.  
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1 The fact that TOC removal remained similar along the three operational stages clearly  
2 showed that the increase in biomass concentration recorded during SII and SIII was  
3 mediated by the enhanced growth of autotrophic microbial communities (microalgae,  
4 cyanobacteria and nitrifying bacteria). Finally, effluent TSS concentrations during  
5 steady state gradually decreased from  $163\pm 83$  mg TSS/L in SI, to  $81\pm 45$  mg TSS/L in  
6 SII and  $26\pm 12$  mg TSS/L in SIII (Figure 4a). The value obtained under steady state in  
7 SIII enabled compliance with the European Directive 97/271/CEE [33].  
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22 The sludge volumetric index recorded at the end of SI in the anoxic tank and  
23 photobioreactor accounted for 95 mL TSS/g and 161 mL TSS/g, respectively (Table 1  
24 and Figure 4b). Surprisingly, the enhanced sedimentation observed during SII, based on  
25 the decrease in the effluent TSS concentrations, was not correlated with the SVI in the  
26 anoxic tank (128 mL TSS/g) or in the photobioreactor (169 mL TSS/g). These high SVI  
27 were likely due to the presence of the filamentous bacteria *Caldilineae* in SI and SII and  
28 *Clostridium* in SI, SII and SIII. However, the decrease in SVI recorded during SIII in  
29 both the anoxic tank and photobioreactor (80 mL TSS/g and 97 mL TSS/g, respectively)  
30 was correlated with low effluent TSS concentrations (Figures 4a and 4b). Overall, SVI  
31 of 50 - 100 mL/g in activated sludge plants are considered an indication of a good  
32 biomass settling [29]. Low SVI were also reported by Alcántara et al. (2015) in a  
33 photobioreactor designed with a continuous biomass recycling. Park et al. (2011) also  
34 reported an increase in microalgae settleability by 20% when implementing biomass  
35 recycling strategies in HRAPs, which confirmed the key of role of this operational  
36 strategy to enhance biomass settling [14][34]. The settling rates of biomass present in  
37 the anoxic tank accounted for 1.86 m/h, 1.20 m/h and 1.44 m/h in SI, SII and SIII,  
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1 respectively. Settling rates of 1.56m/h, 1.02 m/h and 1.47 m/h were recorded for the  
2 biomass present in the photobioreactor in SI, SII and SIII, respectively. An analysis of  
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4 variance confirmed that the biomass present in the anoxic tank exhibited higher settling  
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6 rates than the biomass in the photobioreactor in SI and SII. The results here obtained  
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8 were comparable with those reported by de Godos et al. (2014) and higher than the rates  
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10 obtained by Alcántara et al. (2015) using a similar AA-ABPh [13][14]. Similarly, 80%  
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12 of algal biomass present in a HRAP treating domestic WW at 4 days of HRTs exhibited  
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14 rates higher than 0.4 m/h (Gutierrez et al. 2016) [35].  
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### 22 **3.4 Dynamics of microalgae and bacteria population**

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24 Morphological characterization of microalgae population structure revealed a gradual  
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26 dominance of the genus *Scenedesmus*, which accounted for 46 % of total microalgae  
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28 population in the absence of biogas supply, and for 94-100% when CO<sub>2</sub> was  
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30 supplemented to the wastewater treatment process (Figure 5). *Desmodesmus spinosus*,  
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32 *Pseudanabaena sp.*, *Leptolyngbya benthonica* and *Acutodesmus obliquus* represented  
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34 38%, 30%, 23% and 8% of the total microalgae population in SI, respectively. In SII,  
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36 *Leptolyngbya benthonica* and *Pseudanabaena sp* were gradually replaced by  
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38 *Desmodesmus spinosus* and *Acutodesmus obliquus*, which accounted for 50% and 44%  
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40 of the total population, respectively. Finally, microalgae population in SIII became  
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42 dominated by *Desmodesmus spinosus* (76%) and *Scenedesmus tenuispina* (24%).  
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44 *Scenedesmus* species is commonly found in HRAPs treating domestic WW [36] because  
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46 of their tolerance to high nitrogen and organic matter concentrations [37][38]. This  
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48 study suggests that biomass sedimentation and recycling can contribute to the  
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50 enrichment of monoalgal microalgae species with good settling properties. Previous  
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52 studies in pilot HRAPs conducted with biomass recycling promoted the dominance of  
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1 unialgal cultures [34]. In this context, biomass settling and recycling also resulted in the  
2 dominance of *Micractinium sp* and *Scenedesmus sp* in HRAPs treating RWW with an  
3 external CO<sub>2</sub> supplementation [27].  
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10 DGGE analysis of the bacterial community in the photobioreactor revealed the  
11 occurrence of 10 phyla and 33 bands (Figure 6 and supplementary material Table S1).  
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13 *Proteobacteria*, which are ubiquitous in the environment, was the dominant phylum  
14 with 17 bands of the 33 sequenced. The phylum *Proteobacteria* was the most dominant  
15 with 9, 9, 6 and 12 bands detected in the inoculum, SI, SII and SIII, respectively (Figure  
16 6 and supplementary material Table S1)[39]. The analysis also identified the phyla  
17 *Acidobacteria*, *Verrucomicrobia*, *Firmicutes* and *Actinobacteria* with two bands each,  
18 the phyla *Chloroflexi*, *Cyanobacteria/Chloroplast*, *Gemmatimonadetes*,  
19 *Ignavibacteriae*, *Candidatus Saccharibacteria* with one band and 3 unclassified  
20 bacteria. Bacteria from the phyla *Proteobacteria*, *Acidobacteria*, *Actinobacteria* and  
21 *Firmicutes* were likely responsible for the degradation of organic matter in both the  
22 anoxic and photobioreactor tanks. Bacteria from the above mentioned phyla are  
23 typically found in activated sludge WWTP, autotrophic nitrifying and denitrifying  
24 bioreactors and HRAPs. More specifically, denitrifying bacteria such as *Pseudomonas*  
25 (SIII), *Litorilinea* (SI and SII), *Gp4* (SII) and *Thauera* (SII and SIII) were identified  
26 (Figure 6 and supplementary material Table S1).  
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29 Likewise, nitrifying bacteria belonging to the family *Xhantomonadaceae* (SI, SII and  
30 SIII) and genus *Aeromonas* (SI and SIII), *Aquamicrobium* (SI, SII and SIII),  
31 *Luteliobacter* (SI, SII and SIII), *Thauera* (SII and SIII) and *Gp4* (SII) were detected as a  
32 result on the increased availability of CO<sub>2</sub>.  
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< Figure 6 >

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5 The Shannon-Weiner diversity index (H) for the inoculum (S0) and the population  
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7 established in the different operational stages showed a high bacterial diversity. The  
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9 Shannon-Weiner diversity index typically ranges from 1.5 to 3.5, higher H values  
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11 corresponding to a higher species richness and evenness [16][20]. In this study, H  
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13 indexes of 3.4, 3.5, 3.2 and 3.2 were estimated in the inoculum and in the microbial  
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15 populations established during SI, SII and SIII, respectively (Figure 6). HRAPs treating  
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17 WW typically exhibit H indexes ranging from 3.0 to 3.5, which confirms the high  
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19 robustness and functionality of the microbiology present in algal-bacterial processes.  
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21 Both the H index and the DGGE band profile clearly showed that biogas  
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23 supplementation in SII and SIII stabilized the bacterial community. The analysis of the  
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25 similarity indexes showed a lower similarity between the inoculum (S0) and the  
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27 population in SI (25.4%), than the similarity between the populations in SI and II (63.2  
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29 %) in SII and SIII (41.30%), which indicated a functional specialization to the host  
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31 environment during the experiment [40].  
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### 41 **3.5 Biogas upgrading**

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43 CO<sub>2</sub> supplementation via biogas upgrading was crucial to ensure an efficient  
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45 nitrification in the photobioreactor and further denitrification in the anoxic tank. CO<sub>2</sub>  
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47 removal from biogas in the absorption column averaged 92±2% and 93±2 % during  
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49 steady state II and III, respectively (Figures 7a). H<sub>2</sub>S was completely removed from  
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51 biogas regardless of the operational stage as a result of its higher solubility compared to  
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53 CO<sub>2</sub> (Figure 7b). The results obtained here were in agreement with the REs of 80% for  
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55 CO<sub>2</sub> and 100% for H<sub>2</sub>S reported by other authors in HRAPs devoted to biogas  
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1 upgrading using a similar L/G ratio of  $\approx 10$  (v/v) [12][41]. While CO<sub>2</sub> supplied was  
2 assimilated by nitrifying bacteria and microalgae, H<sub>2</sub>S was rapidly oxidized to SO<sub>4</sub><sup>2-</sup>  
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4 using the O<sub>2</sub> photosynthetically produced in the photobioreactor. In this context, the  
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6 removal efficiencies of SO<sub>4</sub><sup>2-</sup> in the anoxic tank accounted for 92±54% and 16±50%  
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8 during steady state II and III, respectively (Figure 7c). On the other hand, SO<sub>4</sub><sup>2-</sup>-REs of  
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10 -140±58% and -83±60% were recorded in the photobioreactor during steady state II and  
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12 III, respectively, as a result of SO<sub>4</sub><sup>2-</sup> production from H<sub>2</sub>S oxidation (Figure 7b and 7c).  
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14 The DGGE sequencing analysis revealed the presence of the H<sub>2</sub>S degrading strain  
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16 *Pseudomonas frederiksbergensis* NR\_117177, which supported the biological oxidation  
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18 of H<sub>2</sub>S in the system (Supplementary material Table S1) [42][43].  
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#### 29 **4. Conclusion** 30

31 The novel anoxic-aerobic algal-bacterial photobioreactor coupled with a biogas  
32 upgrading unit here evaluated exhibited consistent C, N and P removal efficiencies. CO<sub>2</sub>  
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34 supplementation from biogas was required to overcome the overall IC limitation  
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36 recorded in SI, and supported both an efficient nitrification-denitrification process and  
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38 an enhanced N and P removal by assimilation during SII and SIII. This innovative  
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40 process configuration also supported an efficient biogas upgrading, with CO<sub>2</sub> and H<sub>2</sub>S  
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42 removal efficiencies of 85 and 100 %, respectively. Continuous biomass settling and  
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44 recycling promoted the enrichment of an unialgal culture by the end of the experiment.  
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46 Finally, DGGE-sequencing analysis confirmed that biogas supplementation promoted  
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48 the development of nitrifying, denitrifying and H<sub>2</sub>S degrading bacteria during SII and  
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## Acknowledgments

This research was supported by the Spanish Ministry of Economy and Competitiveness and FEDER EU program (CTM2015-70442-R) the Regional Government of Castilla y León (Project VA024U14 and UIC 71) and INIA (RTA2013-00056-C03-02). The financial support of the program ERASMUS MUNDUS: EURICA and Universidad Nacional Autónoma de Nicaragua (UNAN-Managua) are also gratefully acknowledged.

## Figure captions

**Figure 1.** Schematic diagram of the anoxic-aerobic algal-bacterial photobioreactor set-up coupled with an absorption column for CO<sub>2</sub> supplementation via biogas upgrading.

**Figure 2.** Removal efficiency of (a) TOC, (b) IC, (c) TN, (d) N-NH<sub>4</sub><sup>+</sup> and (e) P-PO<sub>4</sub><sup>3-</sup> in the anoxic tank (▨), aerobic photobioreactor (▩) and overall system (▧) during the steady states achieved in the three operational stages evaluated. Vertical bars represent the standard deviation from replicate measurements during steady state operation.

**Figure 3.** Time course of nitrite (triangles) and nitrate (squares) in the anoxic tank (black) and photobioreactor (white) during the entire experiment. Vertical dashed lines separate the different operational stage evaluated.

**Figure 4.** Time course of (a) TSS concentration in the anoxic tank (◆) and aerobic tank (○) and effluent (×, secondary axis), and (b) SVI in the anoxic tank (■) and photobioreactor (□) during the steady states achieved in the three operational stages evaluated. Vertical dashed lines separate the different operational stages.

**Figure 5.** Microalgae population structure in the photobioreactor during the entire operational period: *Chlorella* (▨), *Pseudanabaena sp.* (▩), *Leptolyngbya benthonica* (▧), *Nitzschia palea* (■), *Scenedesmus tenuispina* (▨), *Desmodesmus spinosus* (▩) and *Acutodesmus obliquus* (▩).

**Figure 6.** DGGE profile of the bacterial community present in the anoxic-aerobic algal-bacterial photobioreactor in the inoculum (S0), stage I (SI), stage II (SII) and stage III (SIII). Horizontal arrows and numbers indicate the most abundant bacterial communities. The name of the samples and the Shannon-Weiner diversity indexes are also depicted in the upper part of the gel.

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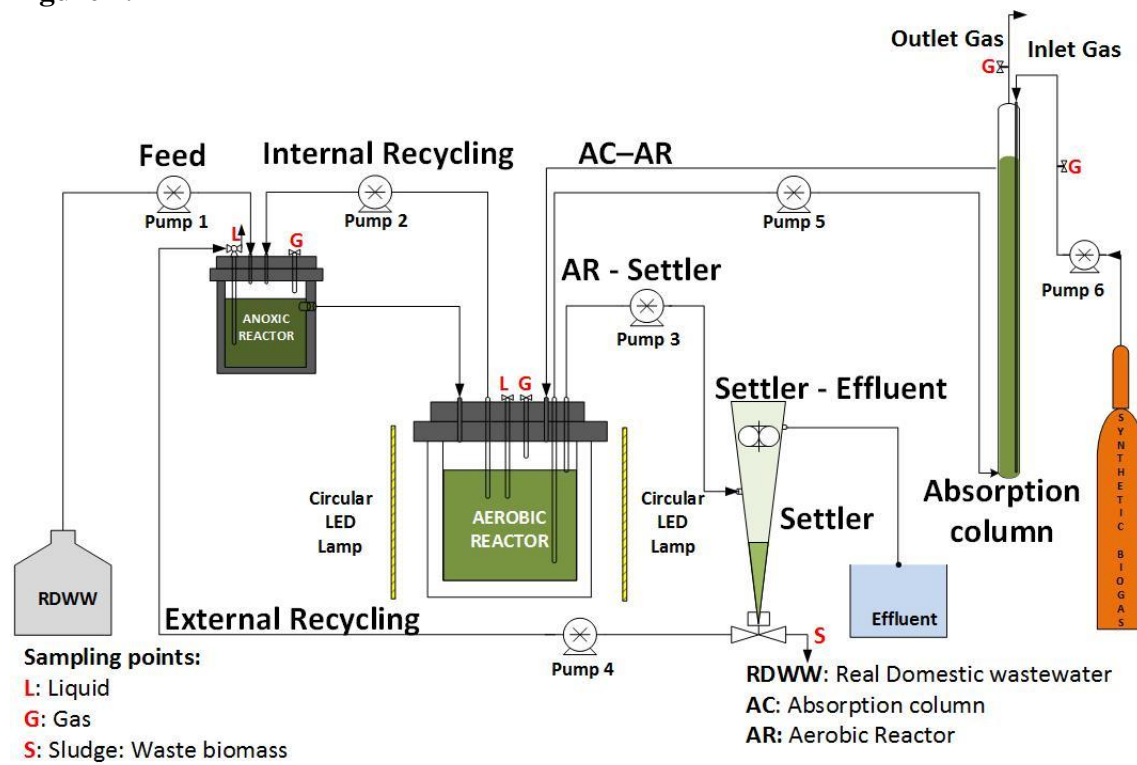
**Figure 7.** Time course of the inlet ( $\blacklozenge$ ) and outlet ( $\Delta$ ) concentrations, and removal efficiency (—) of CO<sub>2</sub> (a) and H<sub>2</sub>S (b), in the absorption column during stage II and III, and (c) removal efficiency of SO<sub>4</sub><sup>2-</sup> in the anoxic tank (▨), aerobic photobioreactor (▩) and overall system (⋯) during the steady states achieved in the three operational stages evaluated. Vertical bars represent the standard deviation from replicate measurements during steady state operation.

**Table 1.** Operational conditions and physical/chemical characterization of the real wastewater and cultivation broth in the anoxic tanks and photobioreactor.

Stage		Wastewater	SI		SII		SIII	
			Anoxic	Aerobic	Anoxic	Aerobic	Anoxic	Aerobic
Operational period (days)		n.a	78		74		56	
HRT (days)		n.a	0.5	1.5	0.5	1.5	0.5	1.5
SRT (days)		n.a	12.5 ± 3.5		11 ± 0.9		10.5 ± 0.5	
Light (μmol/m <sup>2</sup> .s)		n.a	n.a	367±57	n.a	412±15	n.a	395±21
RWW feeding rate (L/d)		n.a	1.8		1.8		1.8	
Internal recycling rate (L/d)		n.a	2.8		2.8		3.6	
External recycling rate (L/d)		n.a	0.5		0.5		0.5	
pH (units)	<i>Light</i>	n.a	7.4±0.3	8.6±0.6	6.9±0.1	8.0±0.7	6.8±0.2	8.9±0.9
	<i>Dark</i>	n.a		7.1±0.3		7±0.2		7.0±0.4
Dissolved oxygen (mg/L)	<i>Light</i>	n.a	0	23.3±4.1	0	22.0±2.0	0	23.0±1.8
	<i>Dark</i>	n.a		6.0±0.6		3.1±1.2		3.9±0.7
TOC (mg/L)		176±26	26±5	20±4	30±4	19±1	23±2	18±2
IC (mg/L)		152±34	48±5	2±1	56±9	15±5	47±4	13±4
TN (mg/L)		106±9	74±10	66±8	32±4	21±3	28±2	18±4
N-NH <sub>4</sub> <sup>+</sup> (mg/L)		93±9	64±4	54±8	32±5	3±1	33±2	3±1
N-NO <sub>2</sub> <sup>-</sup> (mg/L)		n.a	0.01±0.01	5.6±4.0	0.03±0.05	3.1±3.8	0.41±0.68	1.1±1.8
N-NO <sub>3</sub> <sup>-</sup> (mg/L)		n.a	0.04±0.03	0.9±0.9	0.14±0.15	8.9±5.5	0.73±1.25	13.0±3.2
P-PO <sub>4</sub> <sup>3-</sup> (mg/L)		33±8	26±5	16±7	18±3	9±2	18±1	11±2
SO <sub>4</sub> <sup>2-</sup>		39±12	29±7	32±6	51±15	76±11	47±7	55±4
TSS (mg/L)		n.a	1519±252	1216±260	3113±361	2854±324	2480±309	2047±186
SVI (mL/g)		n.a	95	161	128	169	80	97
Air flow (mL/min)		n.a	0	6	0	4	0	2
Biogas (L/day)		n.a	n.a			2.6		2.6
n.a : Not applicable								

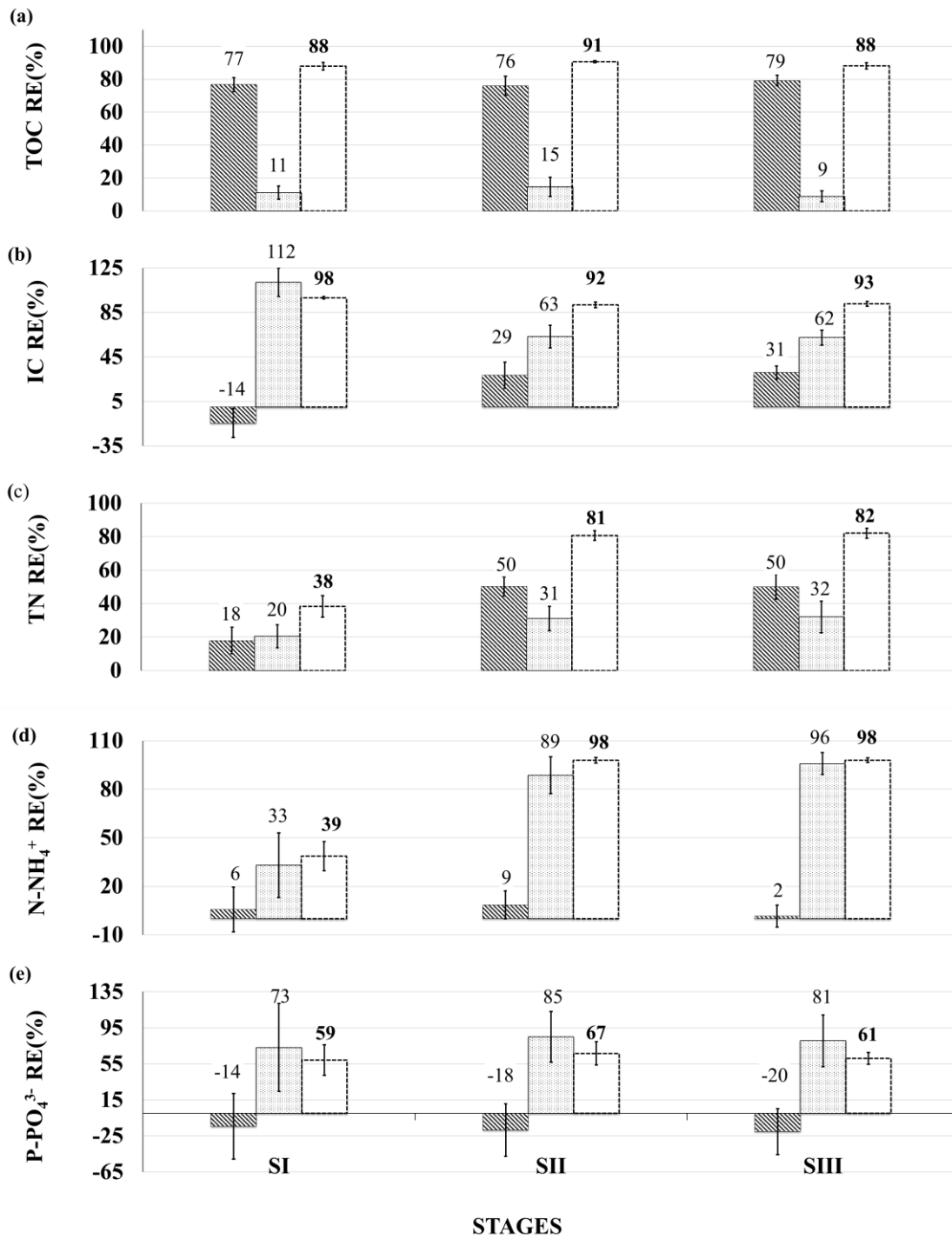


Figure 1.



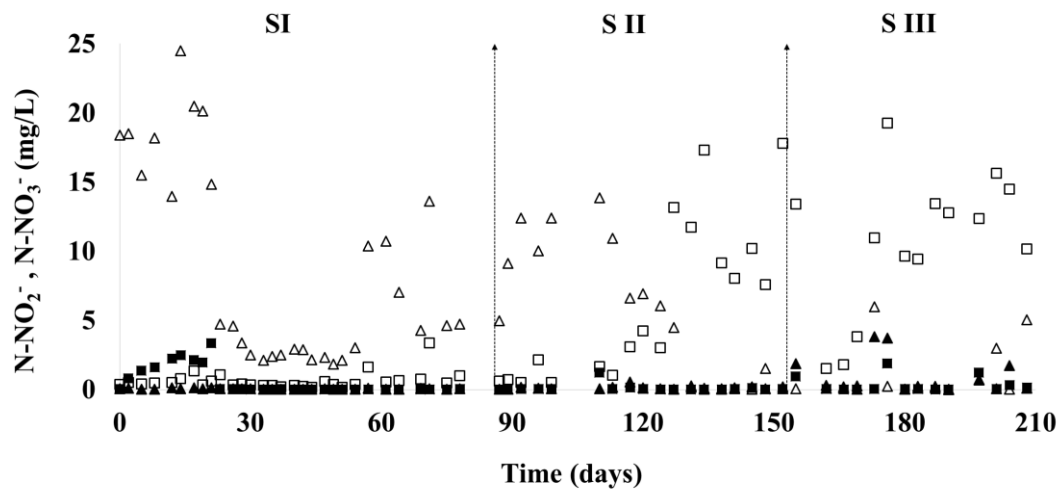
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**Figure 2.**



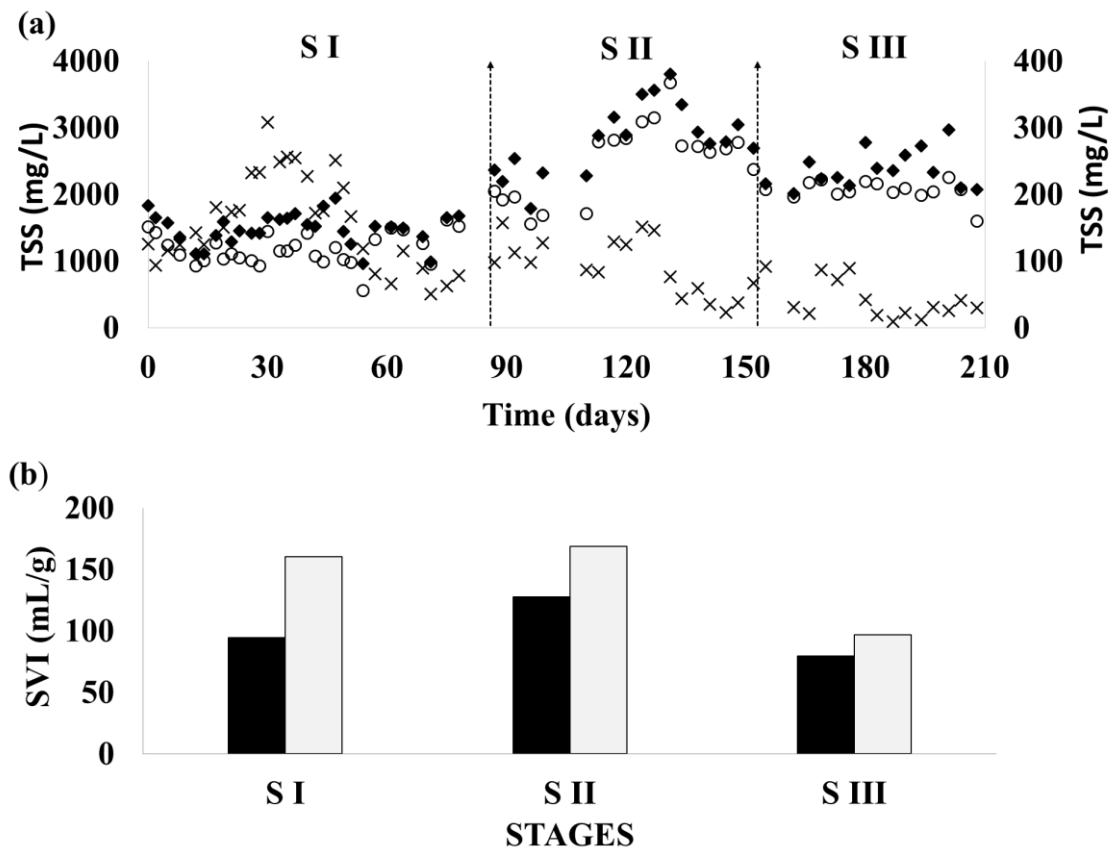
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**Figure 3.**



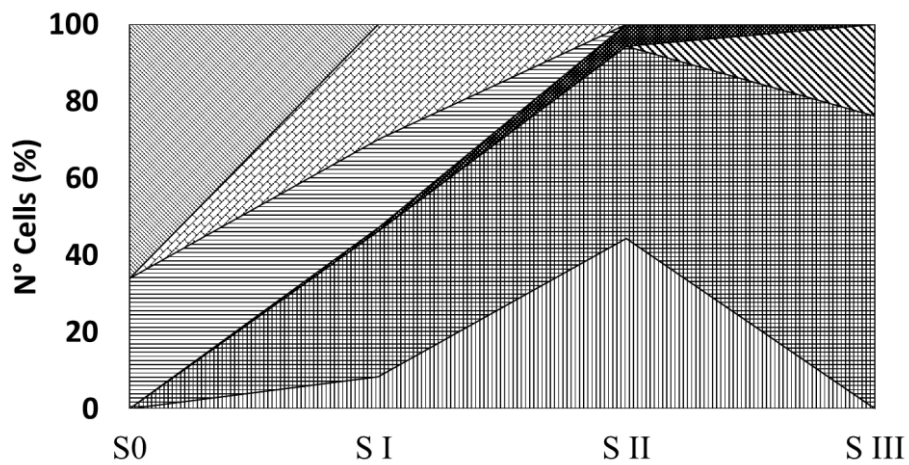
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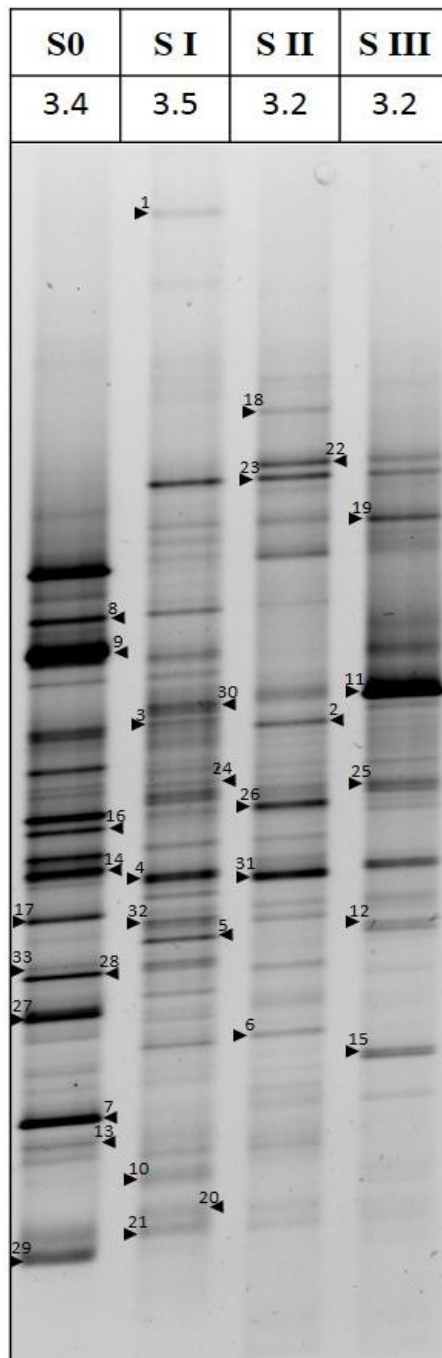
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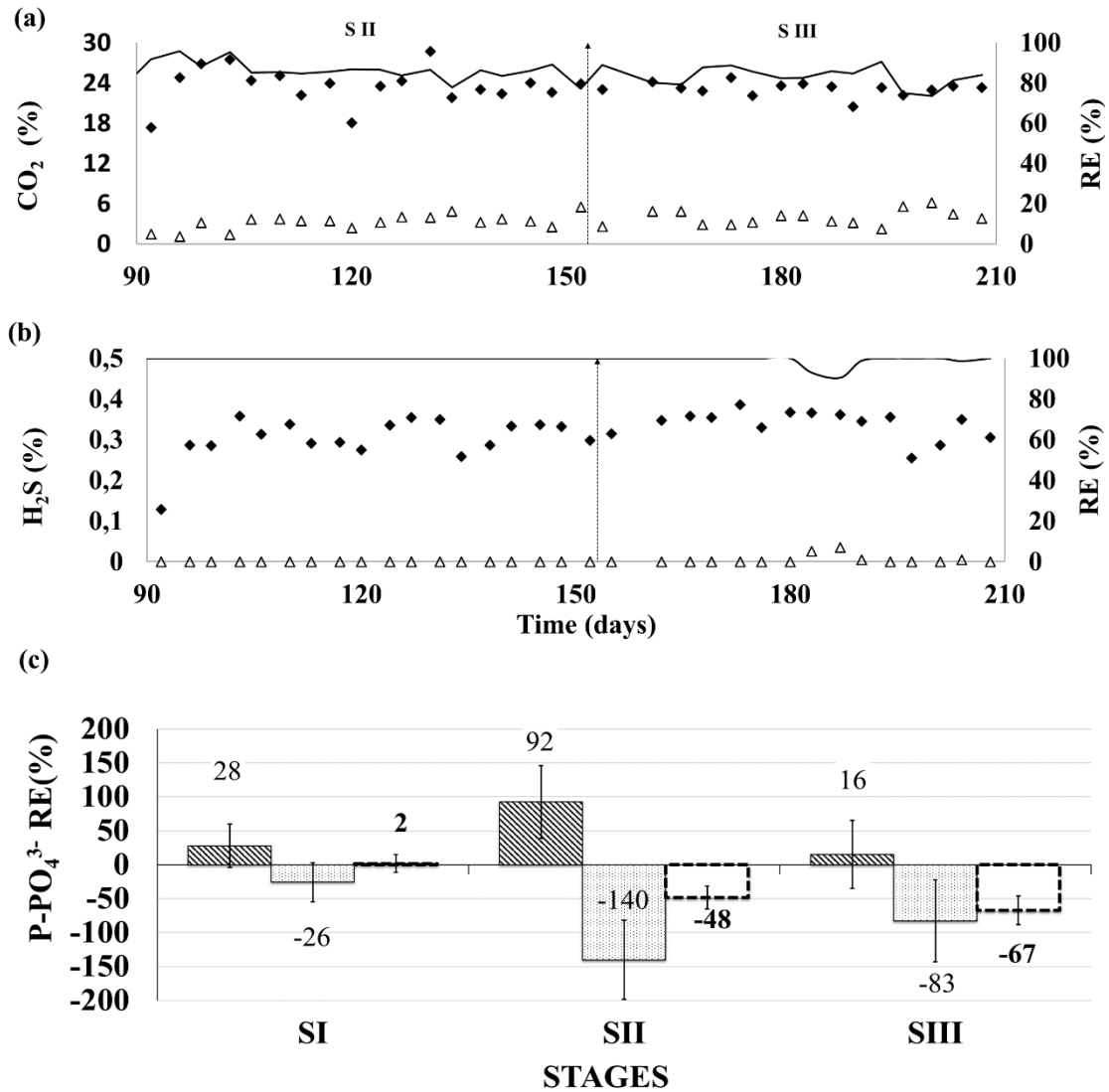
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**Figure 6.**



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**Figure 7.**



**Figure 7.** Time course of the inlet (◆) and outlet (Δ) concentrations, and removal efficiency (—) of CO<sub>2</sub> (a) and H<sub>2</sub>S (b), in the absorption column during stage II and III, and (c) removal efficiency of SO<sub>4</sub><sup>2-</sup> in the anoxic tank (▨), aerobic photobioreactor (▤) and overall system (⋯) during the steady states achieved in the three operational stages evaluated. Vertical bars represent the standard deviation from replicate measurements during steady state operation.

**Supplementary Material**

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